

Extensional Rheology: An Invaluable Tool for Material Characterization

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Rheology as an Analytical Tool

rhe·ol·o·gy /rē'äləjē/

noun:

The branch of physics that deals with the deformation and flow of matter.

- The goal of any rheologist is to relate the rheological properties of a material measured in the laboratory to its molecular structure/architecture
 - ◆ Gain a fundamental insight into material deformation behavior
 - ◆ Develop constitutive models that embody these fundamental structure/property relationships
 - ◆ Predict how newly developed materials will behave to applied deformations during processing and end-product use



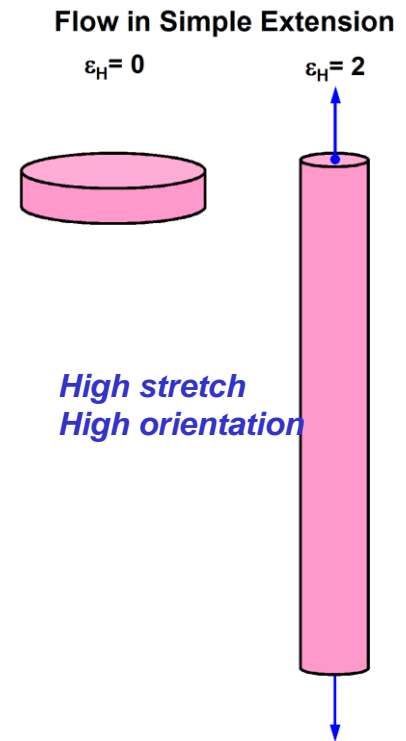
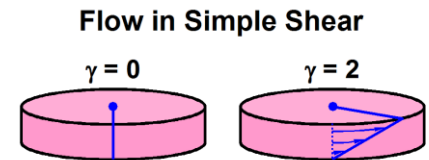
Rheological Characterization of Materials

- Most material deformations are generated with simple shear flows because they are the easiest to generate in the laboratory
- As a consequence, shear rotational rheometers dominate the rheological characterization market
- Although shear rheology has been very useful in establishing fundamental material structure-property relationships, shearing flows generated by rotational rheometers are typically limited to flows in the linear viscoelastic (LVE) regime [small strain, low-rate material deformations] and are unable to distinguish certain polymer macrostructural features
- From an applications standpoint the types of flows witnessed in most polymer processing operations are both rapid and large - nonlinear viscoelastic (NVE) by nature



Extensional Rheology

- Extensional flow refers to a type of flow deformation that involves the elongation, or stretching, of material and is the type of flow that dominates many polymer processing operations
- Crystallization kinetics and final morphology are deeply affected by molecular orientation and stretch induced by flow during polymer processing
- Extensional flow measurements are very useful in polymer characterization because they generate high molecular stretch and orientation flow fields that are very sensitive to the molecular structure (branching) of a polymeric system and are ideal for characterizing the flow induced crystallization (FIC) behavior of melts



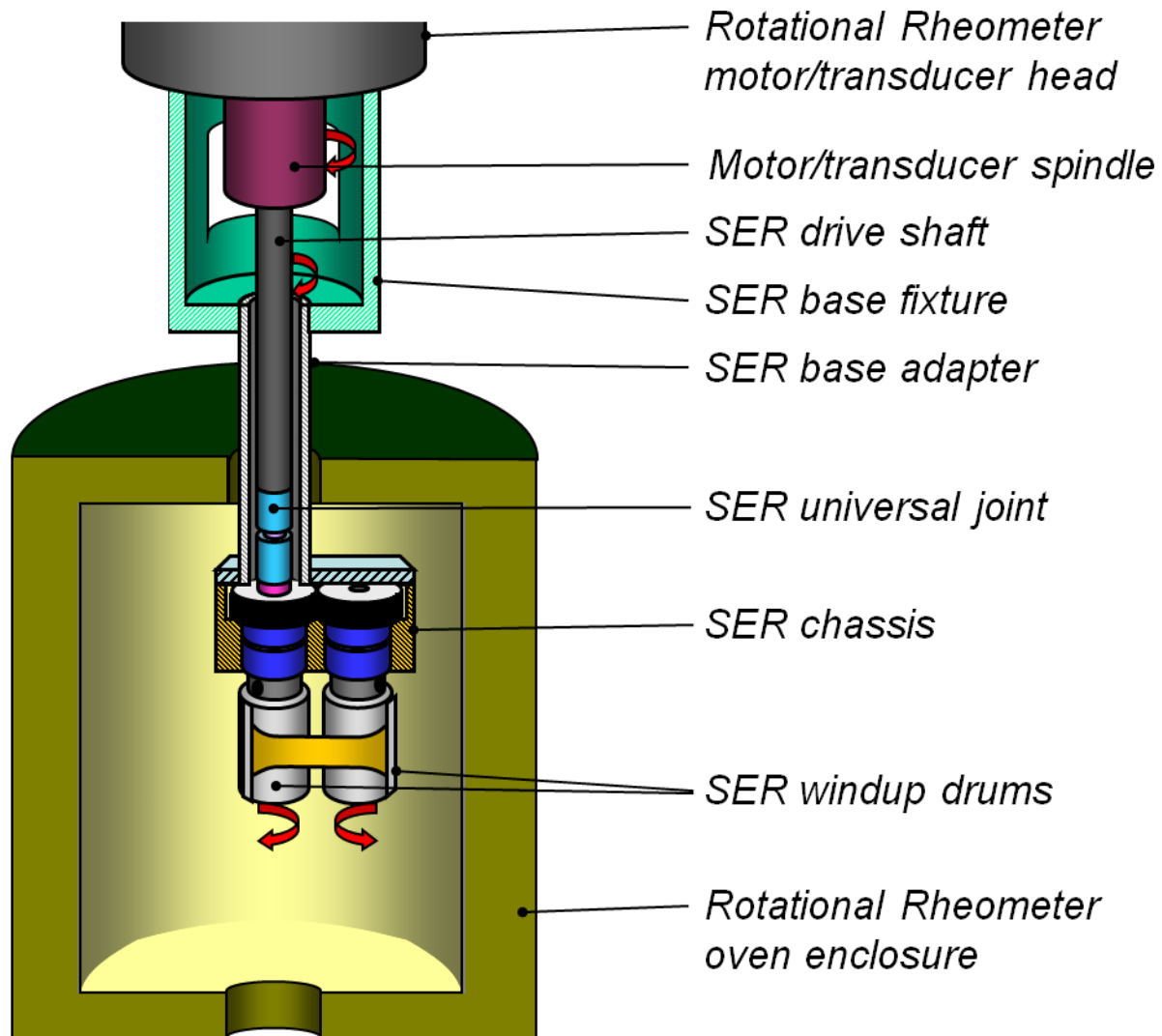
SER Technology

- The SER Universal Testing Platform is a miniature detachable fixture that can convert a conventional CSR or CRR rotational rheometer system into a single universal test station.
- SER Technology translates the precision rotational motion and torque sensing capabilities of a commercial rotational rheometer into precision linear motions and loads.
- By utilizing counter rotating windup drums, linear deformations can be precisely controlled in a fixed plane of orientation which can be viewed at all times during the material deformation process.



SER2 model line

How It Works

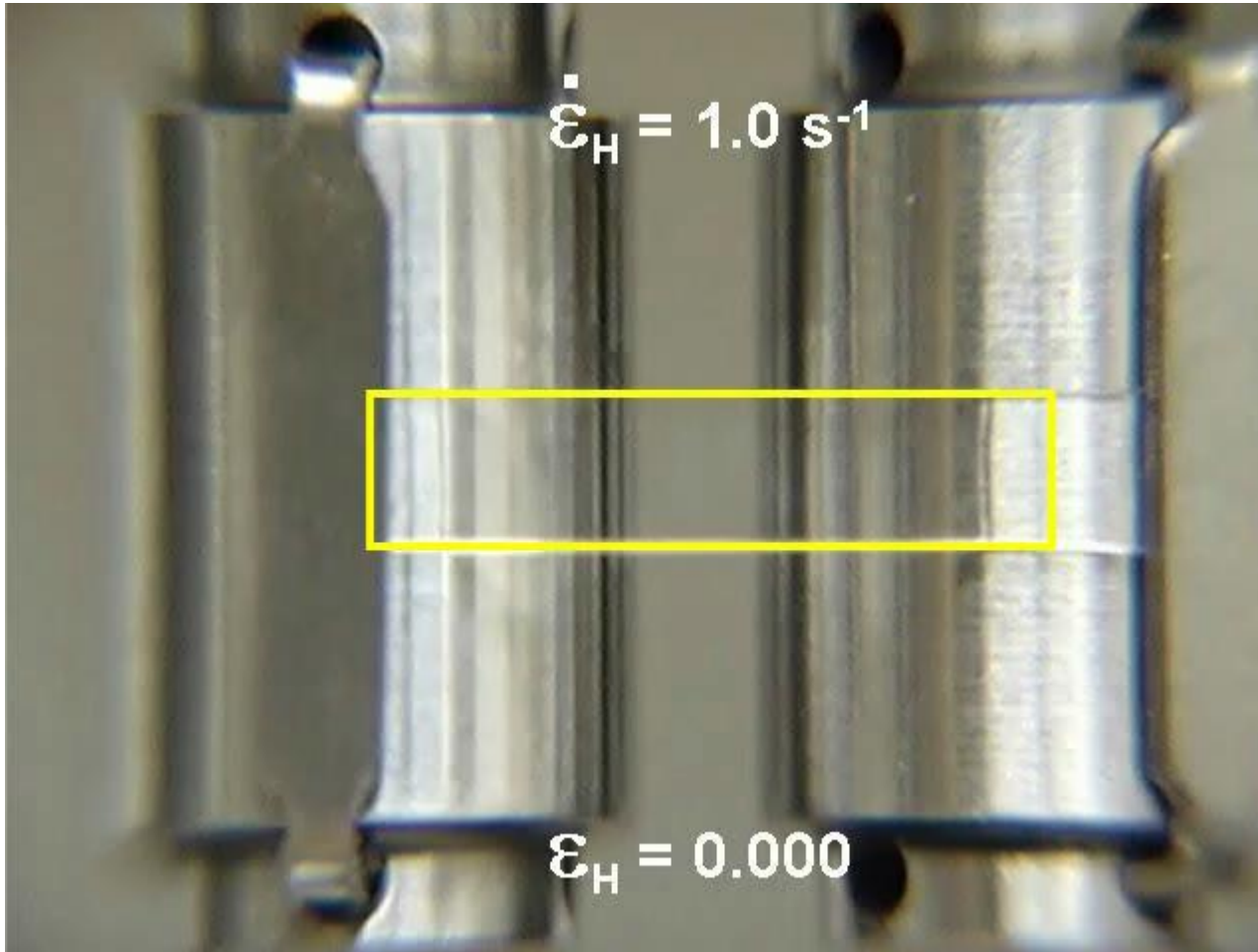


- The rotational motion of the rheometer spindle drives the counter rotation of the dual windup drums.
- Hence, a sample attached to the drum surfaces experiences a controlled *linear* deformation all within the confines of the oven enclosure.



True Strain Rate Validation

Frame Sequencing Videography



 - Indicates Theoretical Width Dimension

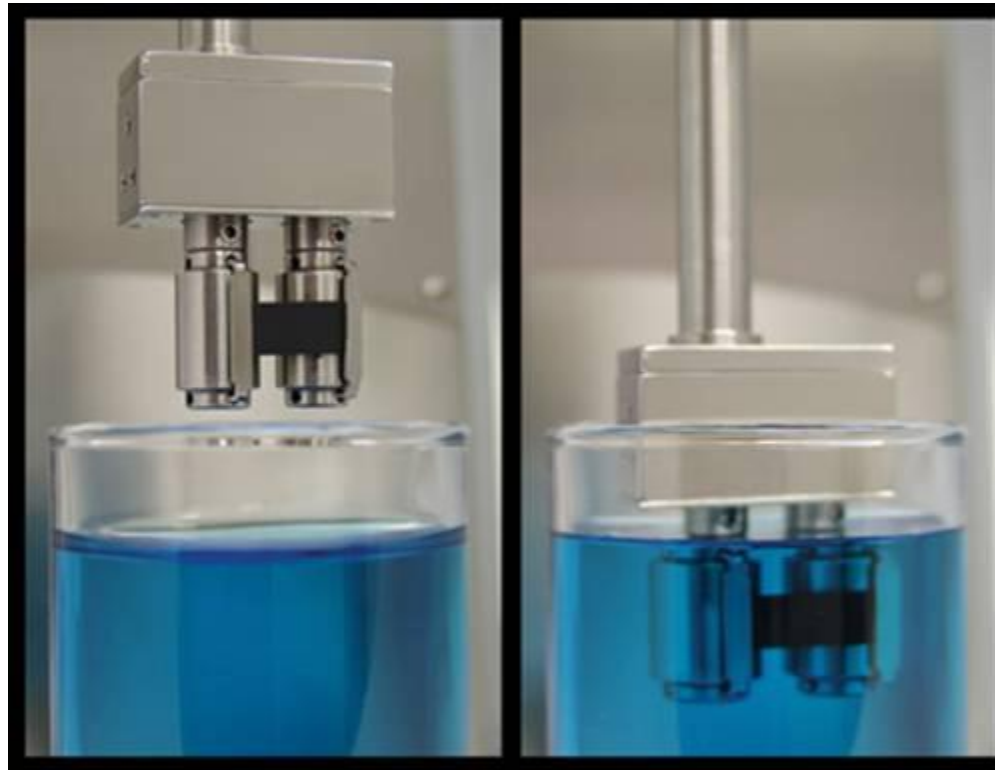
Theoretical width dimension expression:
 $W/W_0 = [\exp(-\epsilon_H)]^{1/2}$

- Note the excellent agreement between the actual and theoretical width dimension evolution



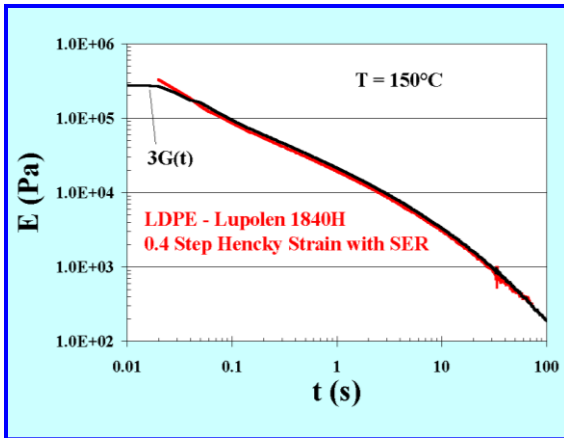
Fluid Immersion Capabilities

- Because both of the detachable drums are cantilevered and suspended from the SER2 base chassis, the SER2 models that are configured for use on controlled stress/strain rotational rheometers are capable of fluid immersion testing... *Perfect for testing molten polymers susceptible to sag effects over long periods of time.*



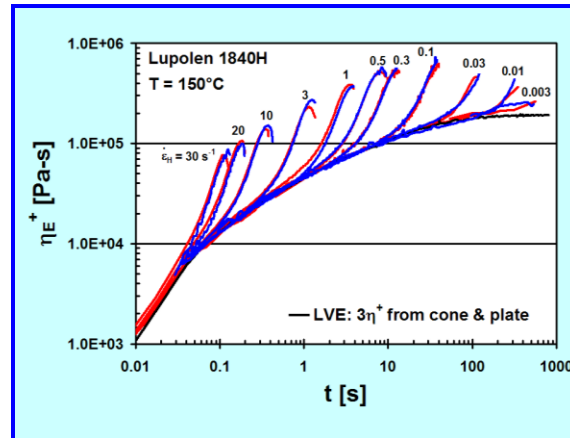
Extensional Rheology

LVE

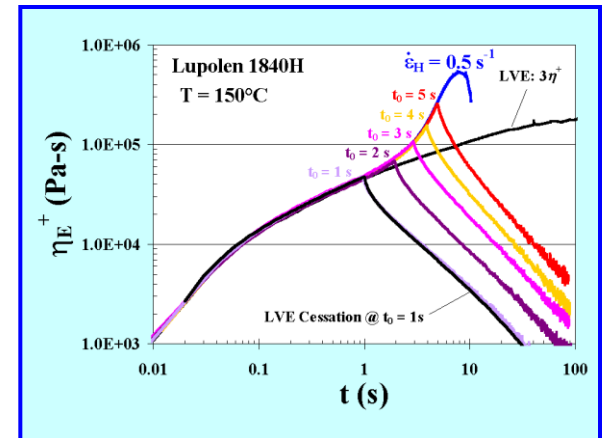


Step Extension

LVE & NVE

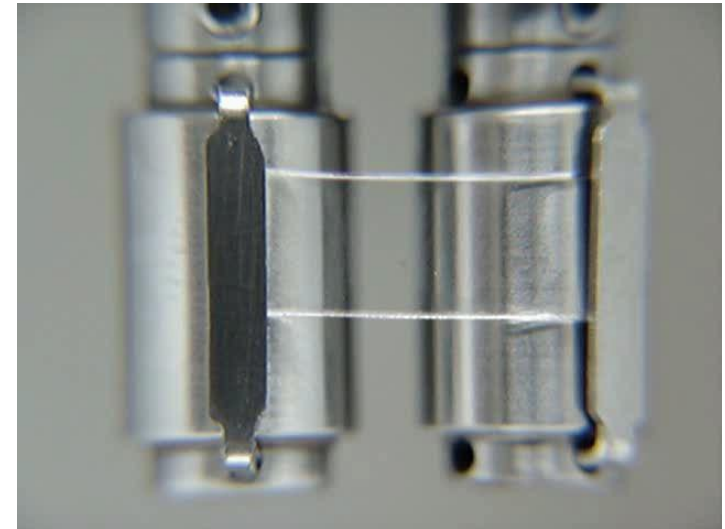


Tensile Stress Growth



Cessation of Extension

- Sample sizes less than 150mg can be used to characterize LVE & NVE properties at steady Hencky strain rates up to 30s^{-1}
- Provides analytical insight with regard to
 - ◆ molecular architecture, size, and structure
 - ◆ processing behavior
- *Applications:* polymer melts, uncured elastomers, TPE melts, highly viscous/semi-solid foodstuffs



FIC Studies in Uniaxial Extension

■ Part 1: Butyl

- ❖ Tensile Stress Growth and Cessation of Uniaxial Extension Experiments
- ❖ Bubble Instability in Unaxial Extension
- ❖ Flow Birefringence

■ Part 2: Linear Polyethylene

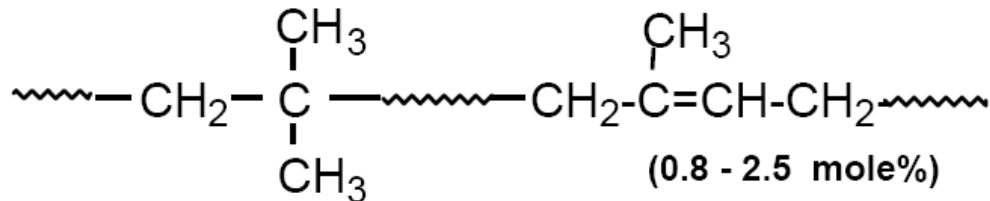
- ❖ Tensile Stress Growth and Cessation of Uniaxial Extension Experiments at Temperatures Near the Melt State
- ❖ Flow Birefringence



Part 1: Butyl Elastomer

- Butyl elastomer (IIR) is the copolymer of isobutylene and a small amount of isoprene, typically in the order of 2%

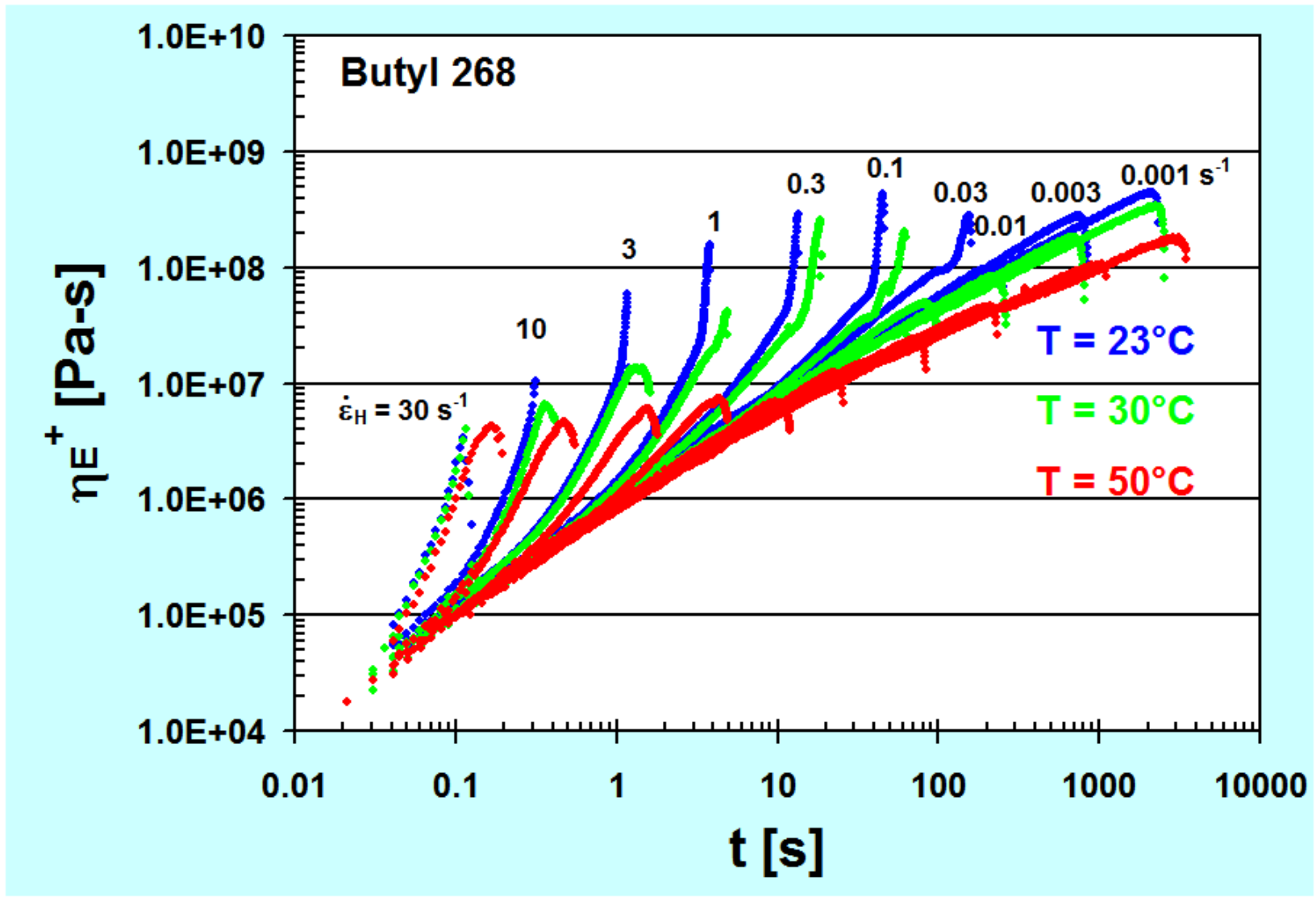
Structure of Butyl Rubber



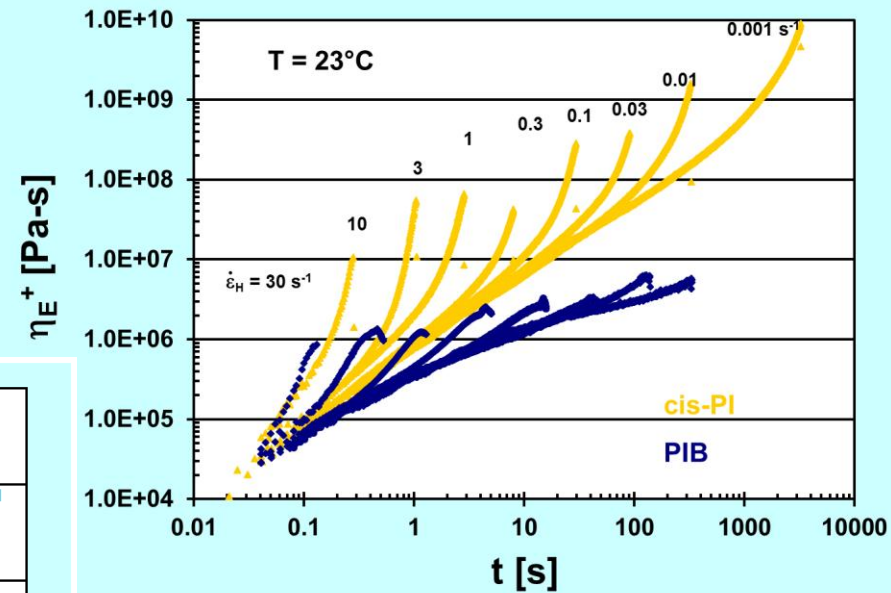
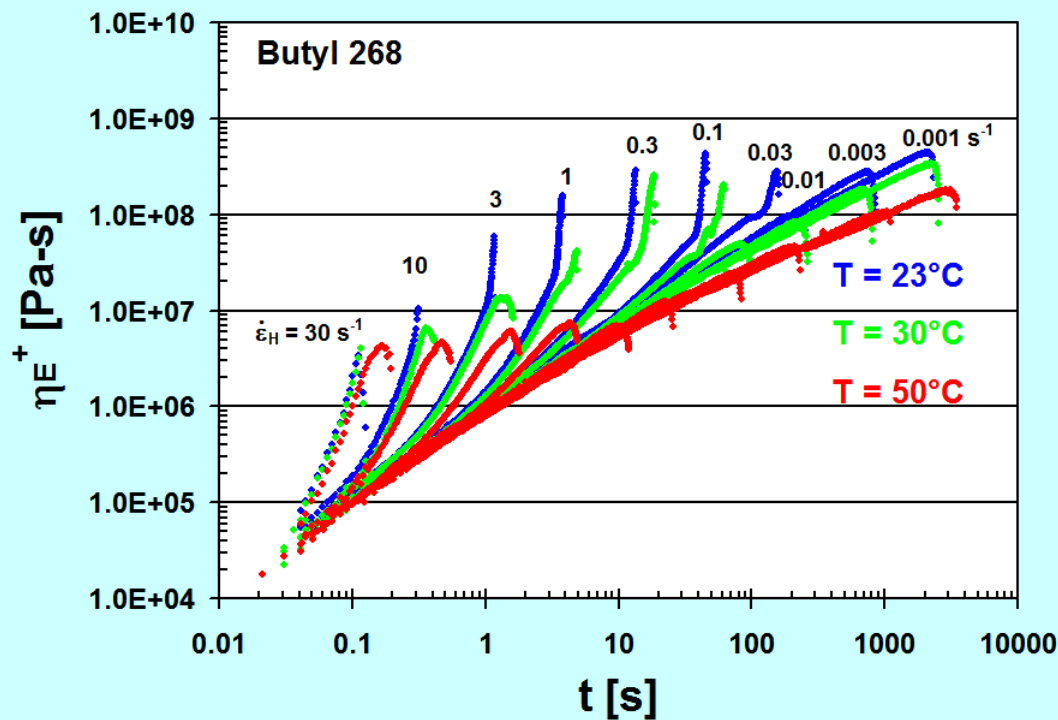
- Due to its gas impermeability and resistance to heat and oxidation, butyl elastomers find application in tire innerliners, innertubes, curing bladders and envelopes, and other specialty applications where air retention and resistance to heat and oxidation are desired
- Because of its gas impermeability, air voids are a common processing issue associated with butyl elastomers



Part 1: Tensile Stress Growth – Butyl

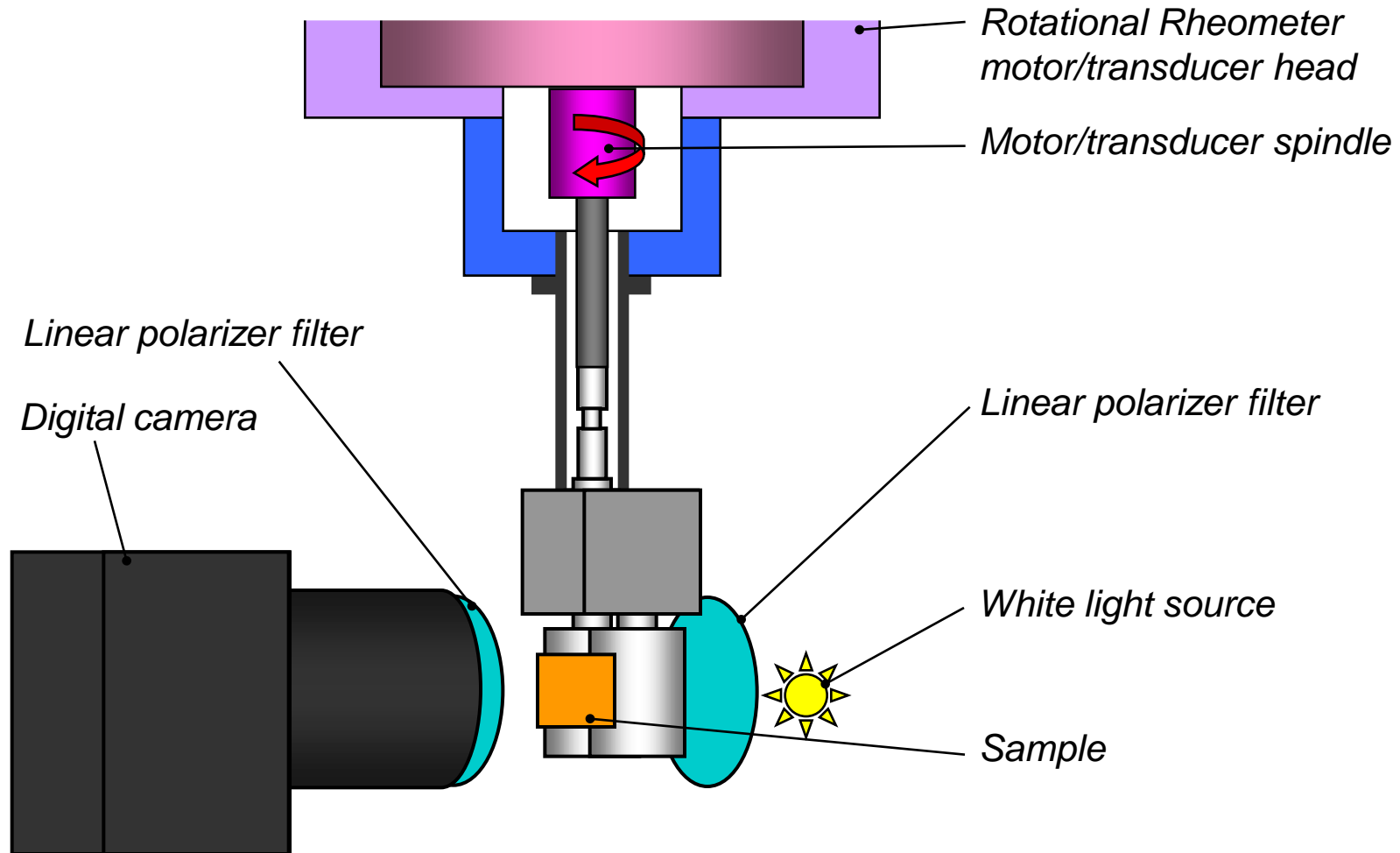


Part 1: Tensile Stress Growth



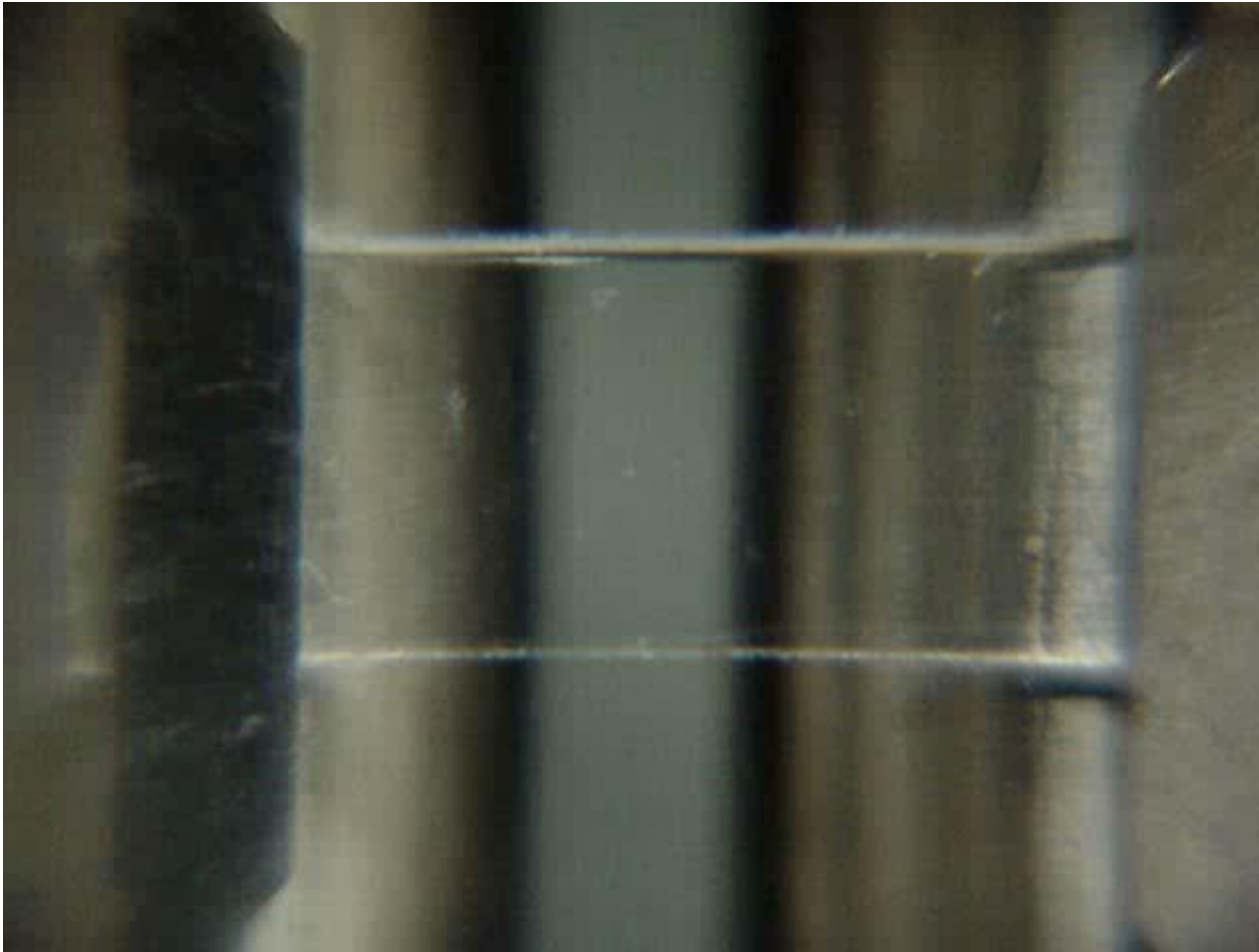
Note how the extensional behavior of Butyl at the higher temperature resembles the extensional behavior of a typical PIB, while at lower temperatures it resembles the behavior of a typical cis-PI

Part 1: Flow Birefringence

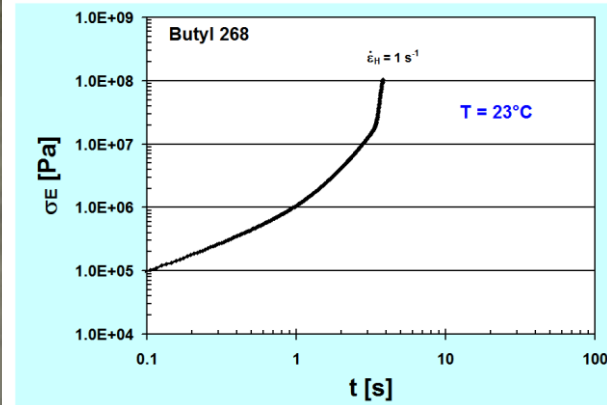


■ Because the deformation remains in a fixed plane and in a well-defined stretch zone, rheo-optical measurements can easily be performed with the SER

Part 1: Flow Birefringence - Butyl in Stress Growth



Uniaxial Extension



Hencky strain rate = 1.0 s^{-1}

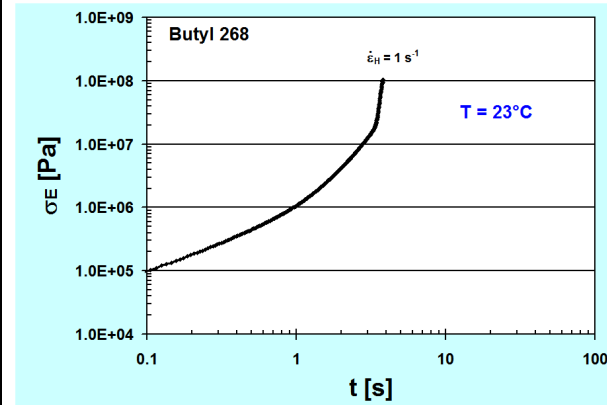
- As the polarized ambient light passes through the sample, the refractive index of the stretching specimen changes as a function of molecular orientation and the onset of FIC



Part 1: Flow Birefringence - Butyl in Stress Growth



Uniaxial Extension



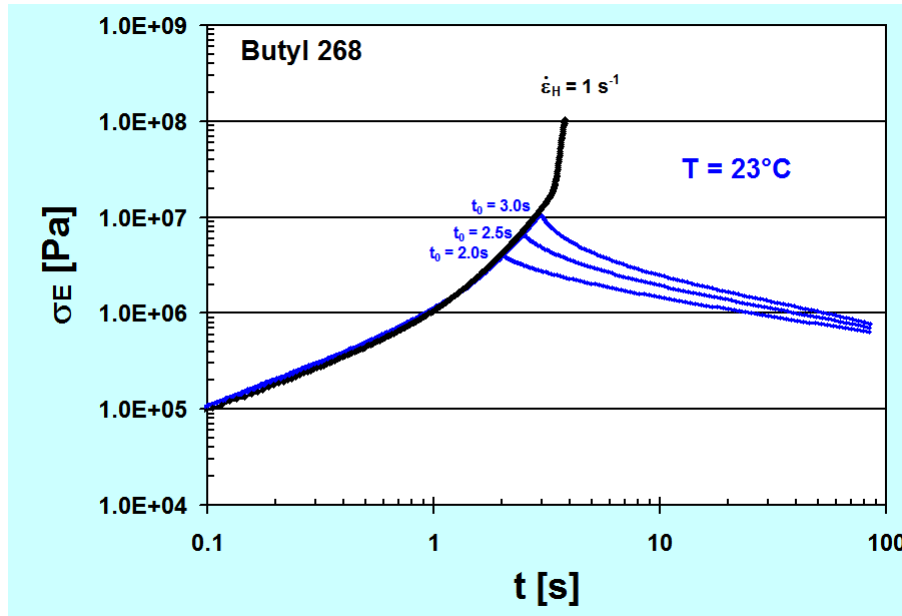
Hencky strain rate = 1.0 s^{-1}

- As the polarized white light source passes through the sample, the refractive index of the stretching specimen changes as a function of molecular orientation and the onset of FIC

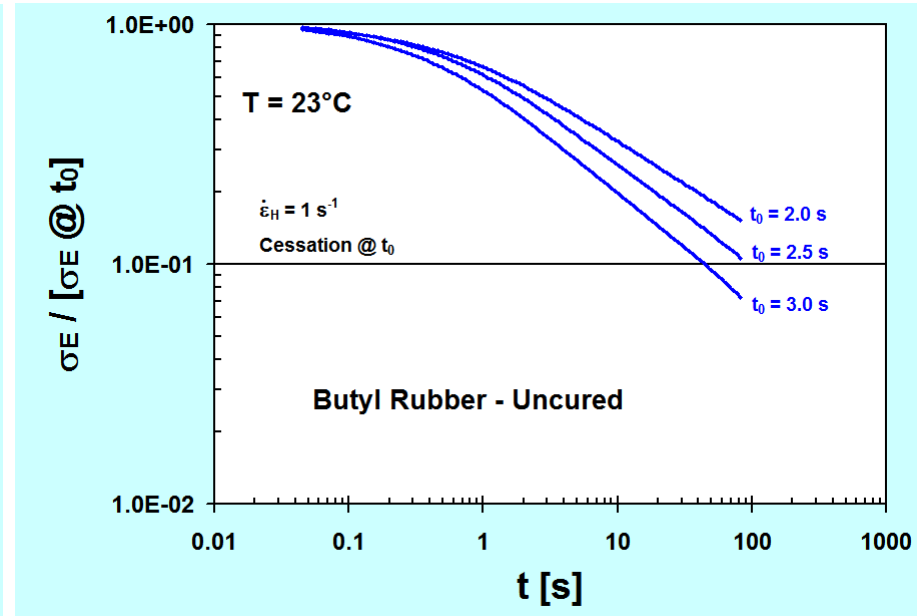


Part 1: Flow Birefringence - Cessation of Extension

Hencky strain rate = 1.0 s^{-1}
Flow Stopped @ t_0



Tensile stress growth and relaxation



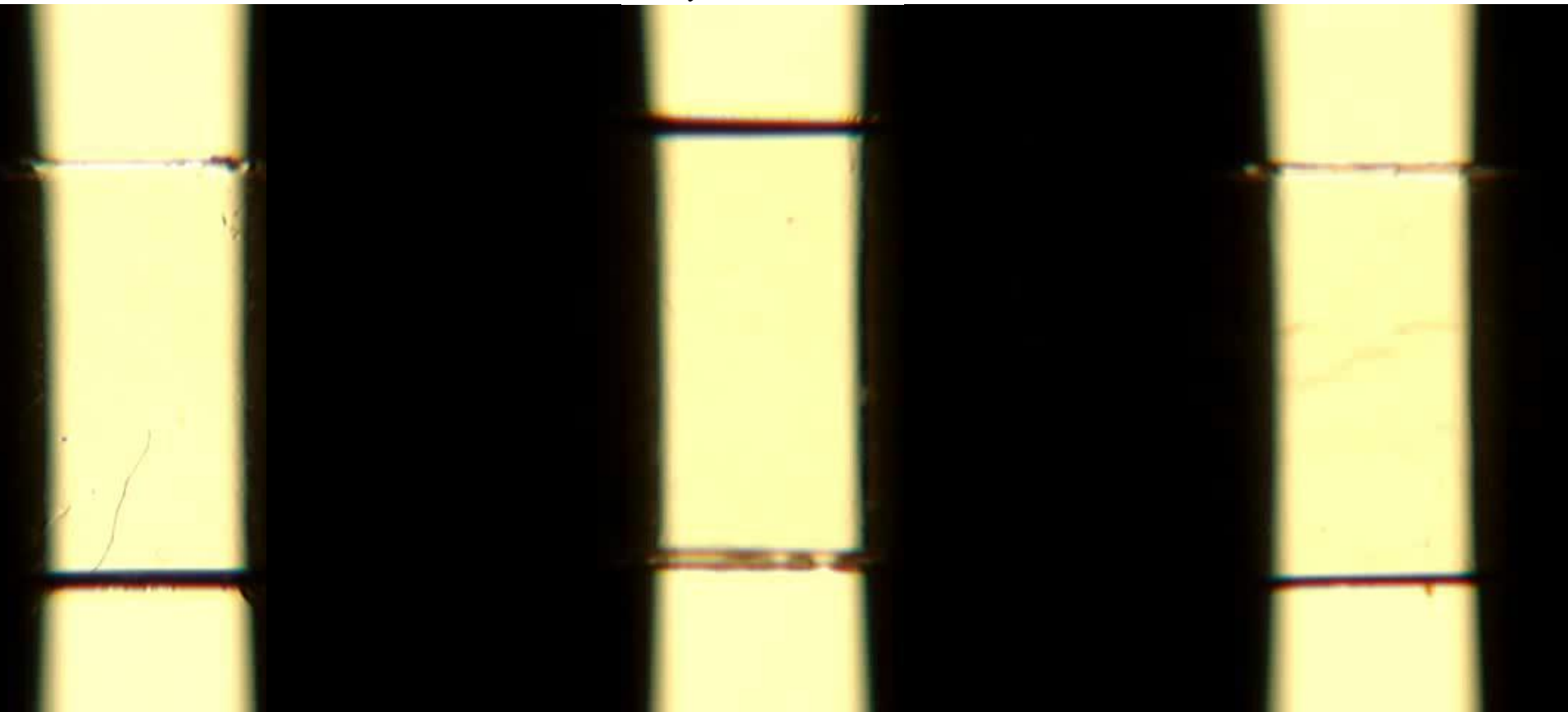
Relative relaxation after t_0

- Note that the degree of relative relaxation increases with increasing deformation history due to relaxation subsequent to FIC



Part 1: Flow Birefringence - Cessation of Extension

Hencky strain rate = 1.0 s⁻¹



$$\epsilon_H = 2.0$$

$$\epsilon_H = 2.5$$

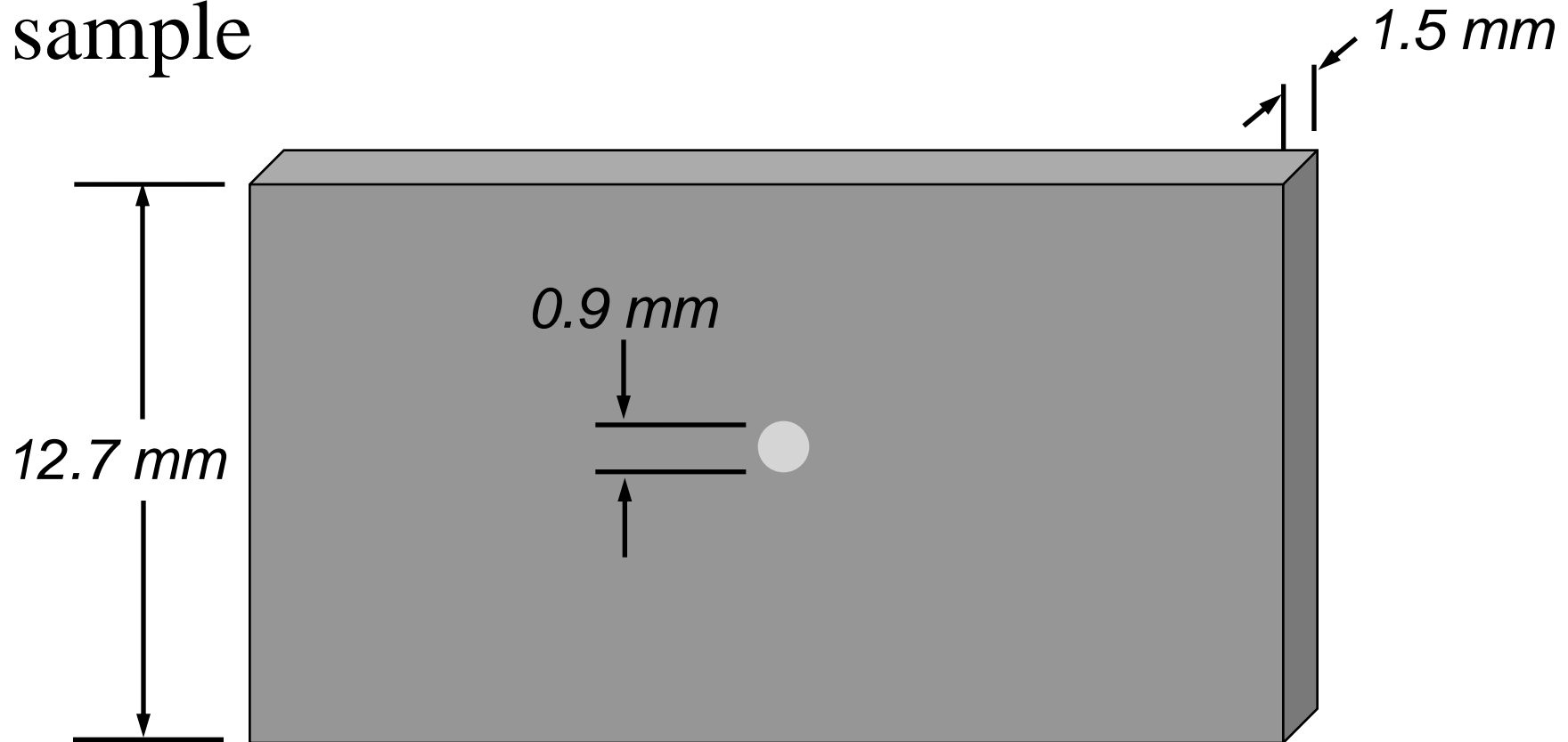
$$\epsilon_H = 3.0$$

- Note the evolution of the color fringes during stress relaxation



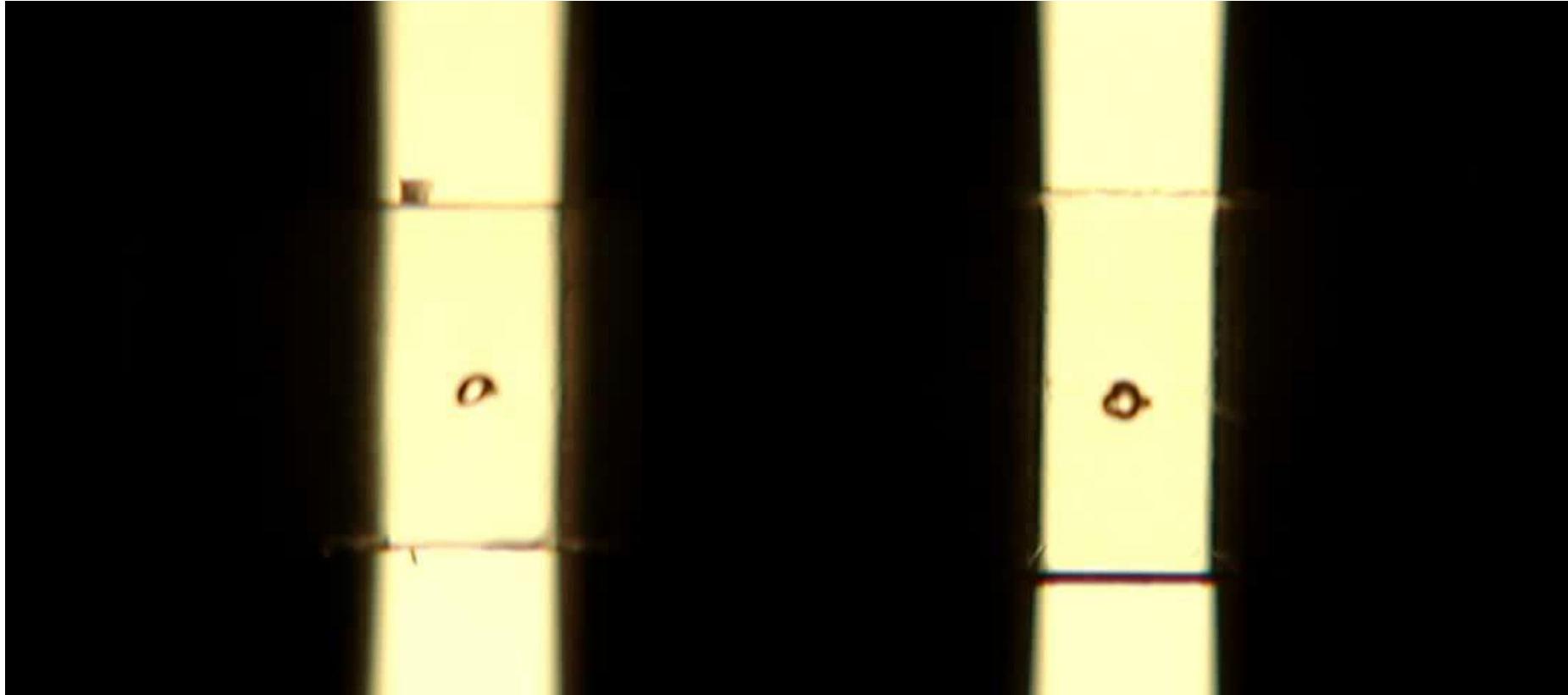
Part 1: Effect of Strain on Bubble Stability

- Samples were prepared with an air bubble void contained within the center of the sample



Part 1: RheoOptics - Effect of Voids

Hencky strain rate = 1.0 s⁻¹



$\epsilon_H = 1$

$\epsilon_H = 2$

- Note how the larger deformation exceeds the critical strain for the onset of bubble instability which subsequently leads to cleaving of the sample

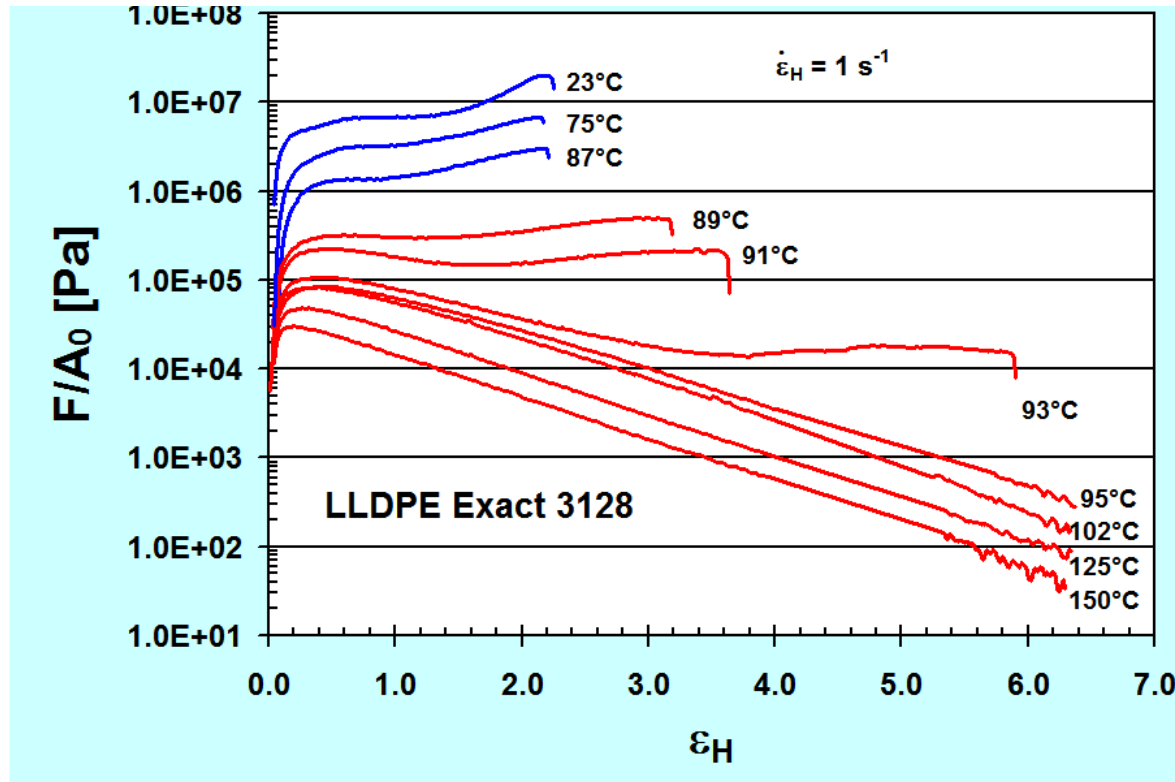
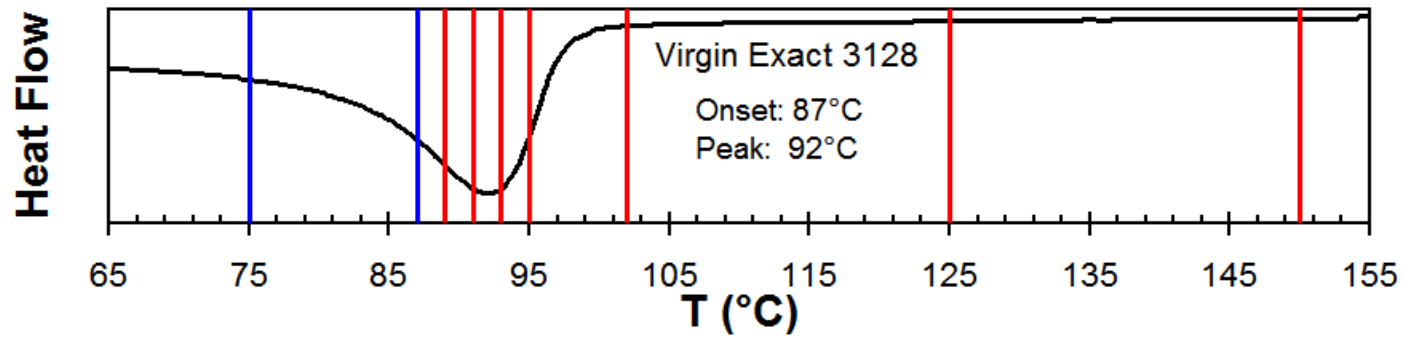


Part 2: Materials

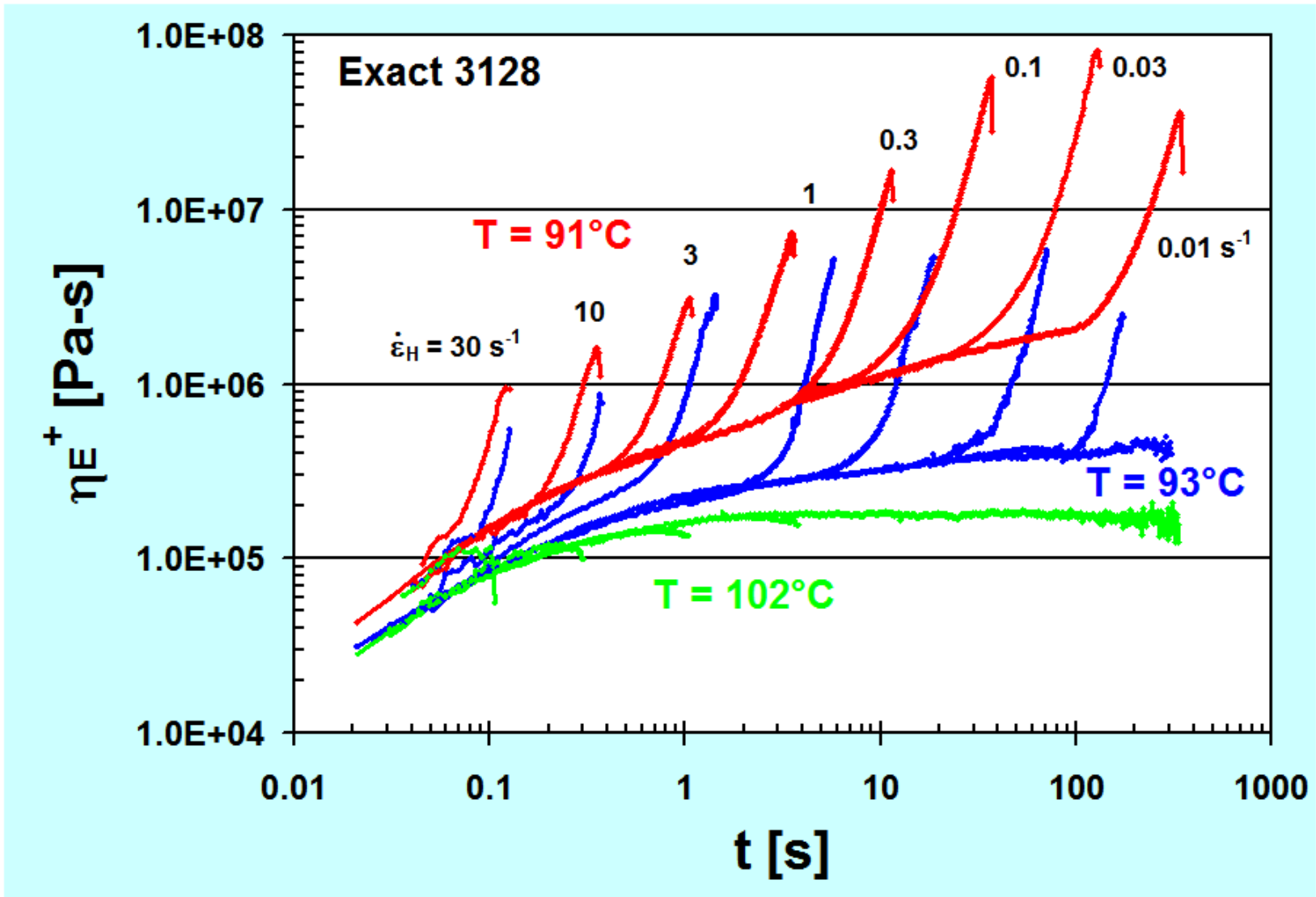
- Because of the higher degree of crystallization that can be achieved in the solid state, linear polymers are particularly sensitive to extensional flows very near the melt temperature.
- Commercial Linear Polyethylenes:
 - ◆ Exact 3128: Film Grade m-LLDPE (ExxonMobil), MFI = 1.2
 - ◆ 58G: Blow Molding Grade HDPE (Nova Chemicals), MFI = 0.95



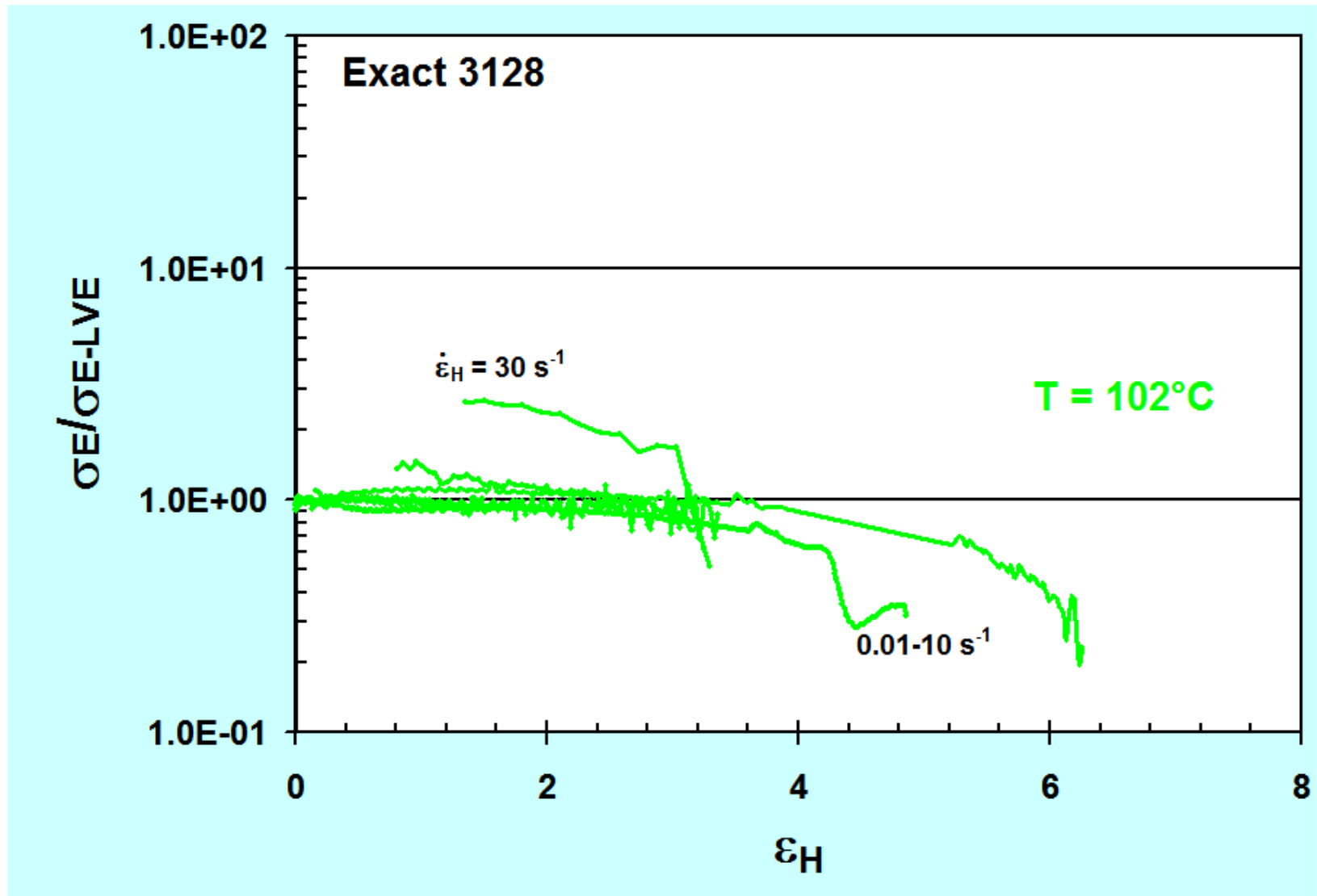
Part 2: FIC & Tensile Stress Behavior – m-LLDPE



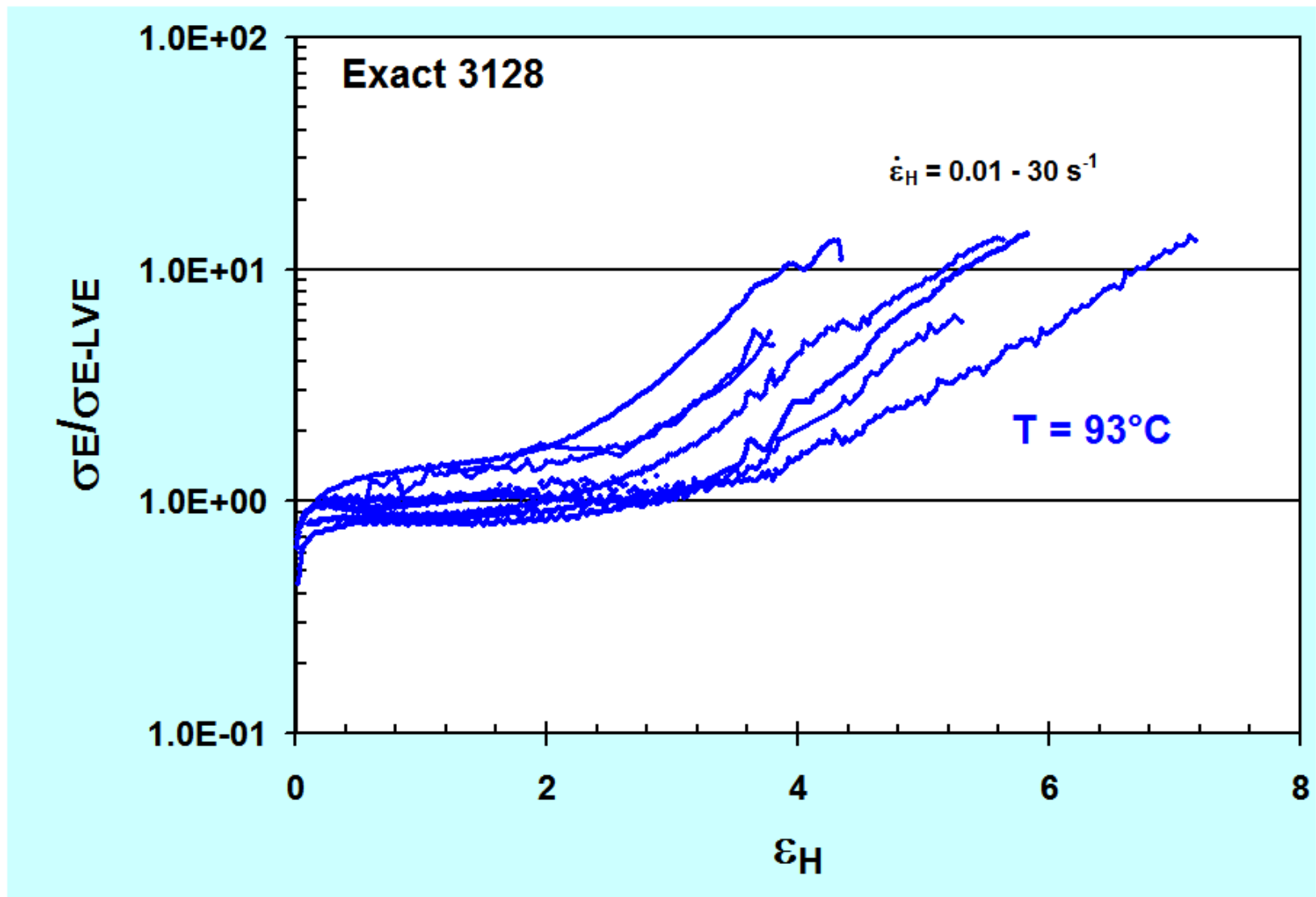
Part 2: FIC & Tensile Stress Behavior – m-LLDPE



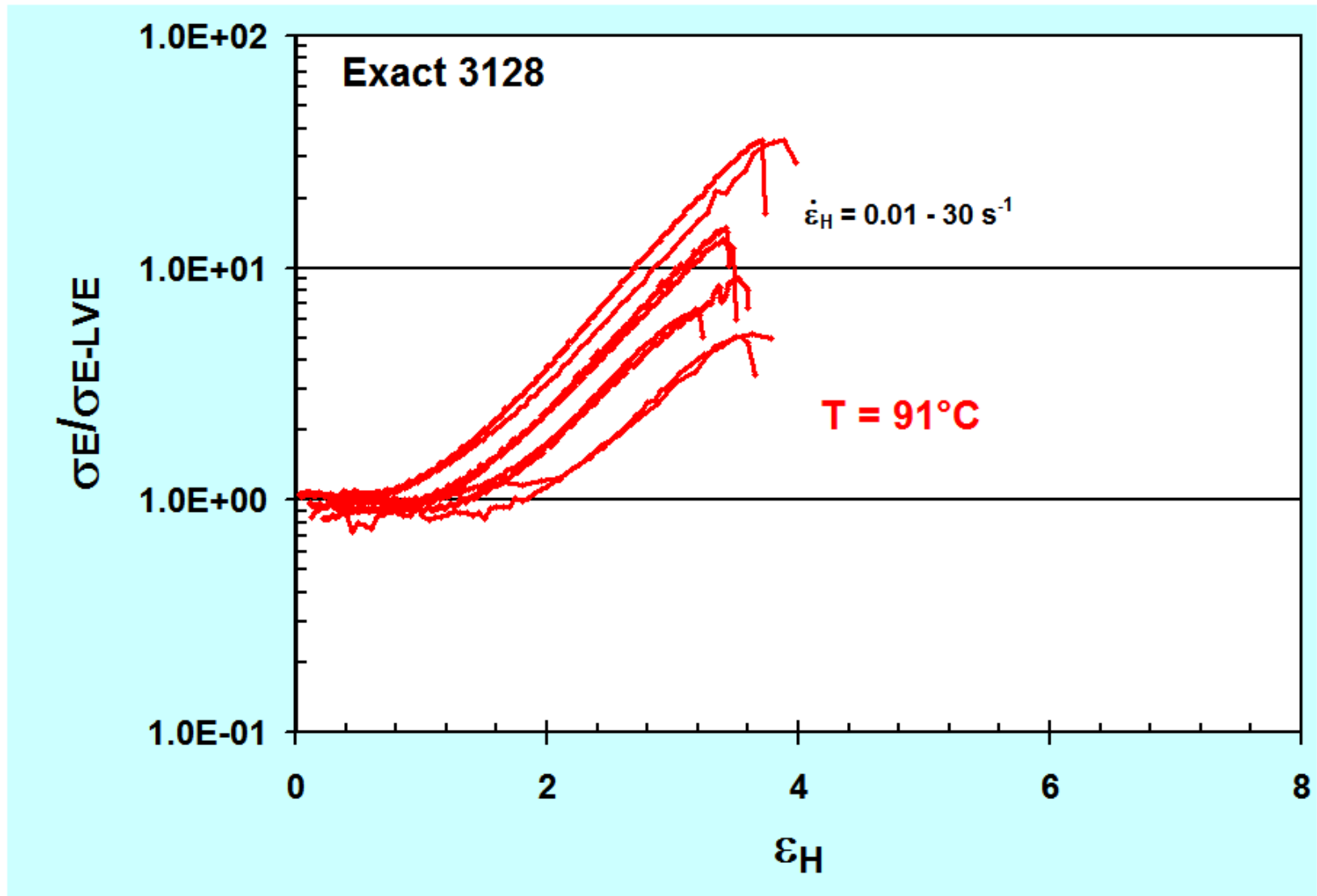
Part 2: Strain Hardening Behavior – m-LLDPE



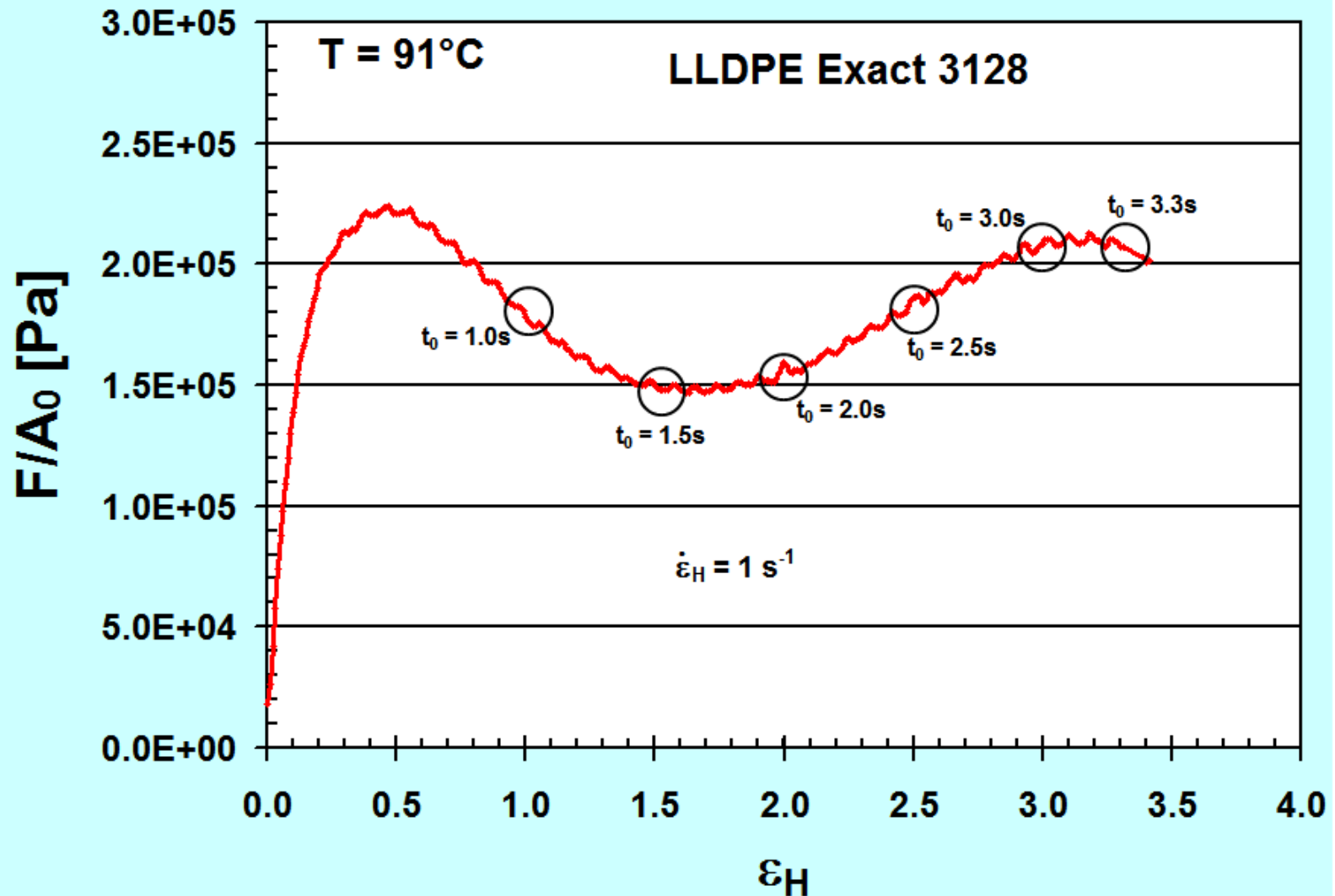
Part 2: Strain Hardening Behavior – m-LLDPE



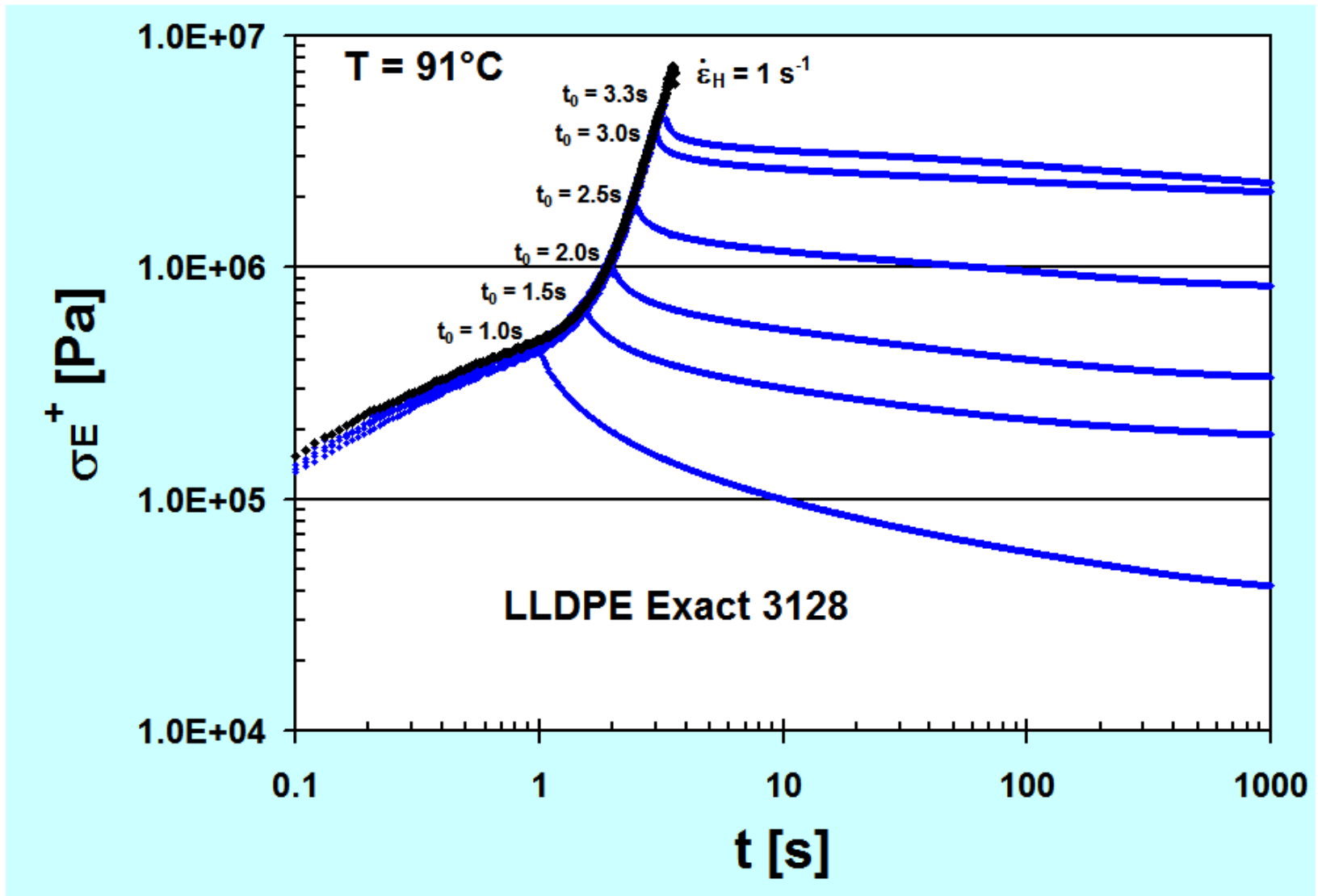
Part 2: Strain Hardening Behavior – m-LLDPE



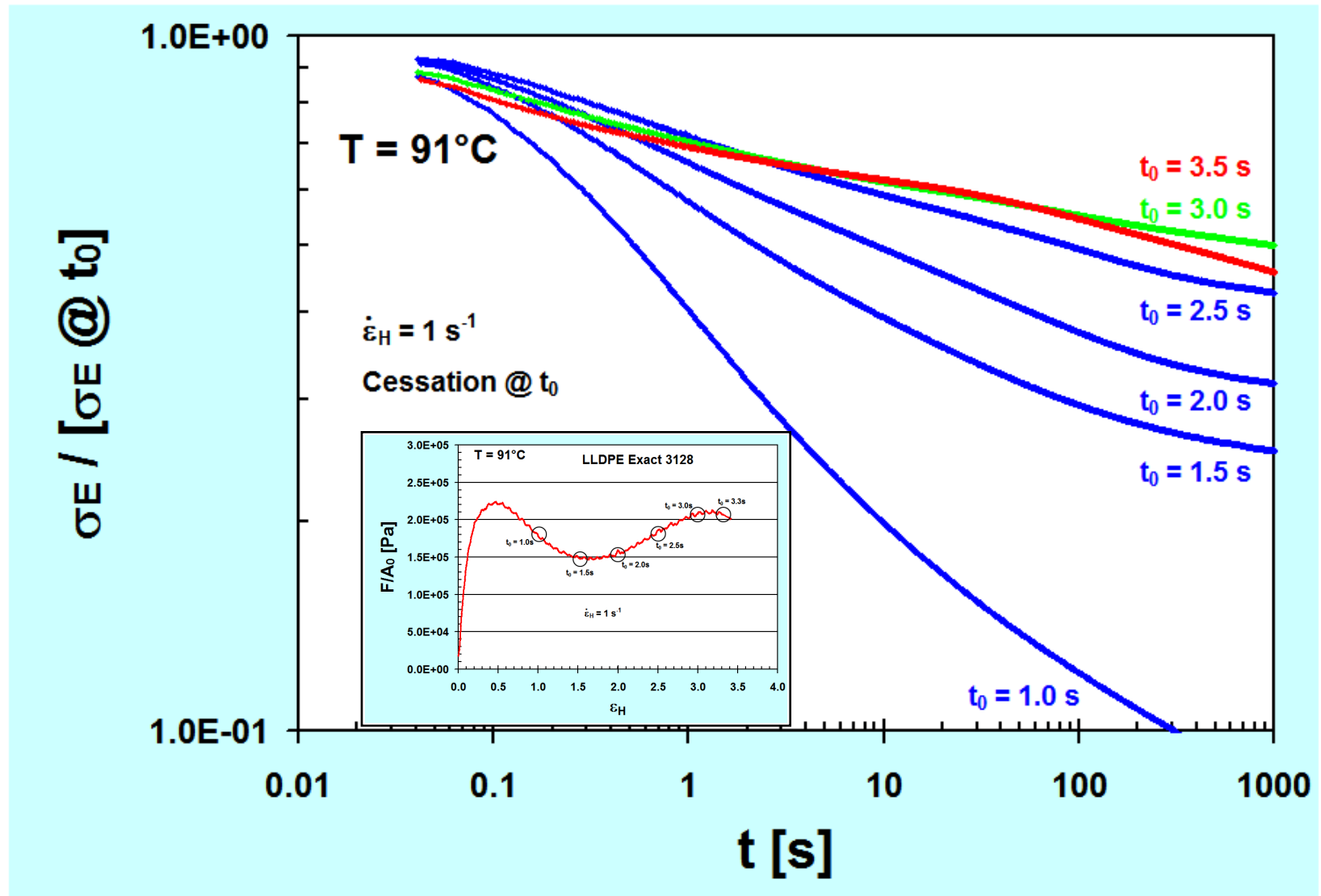
Part 2: Stress vs. Strain - 91°C @ 1s⁻¹



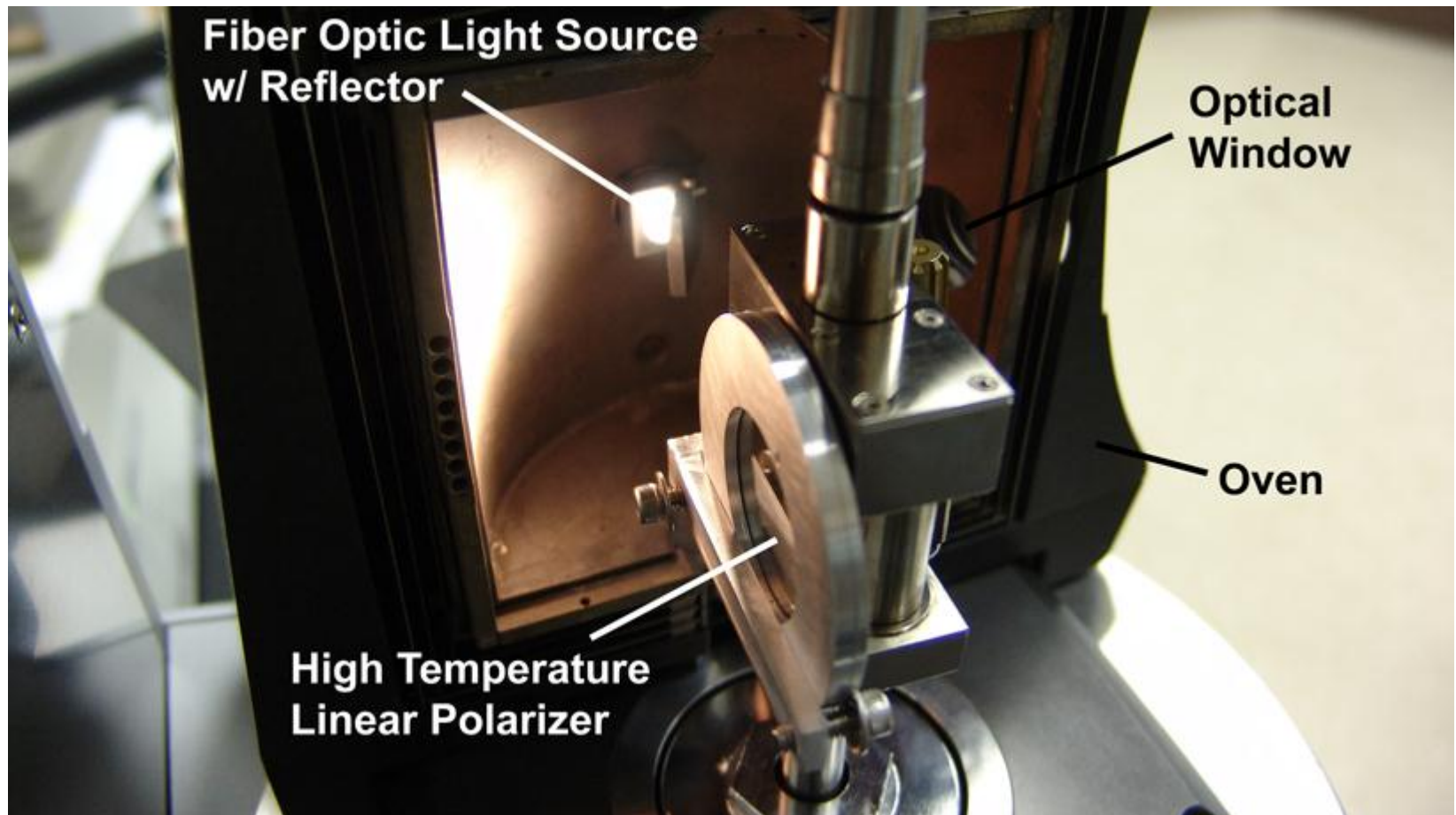
Part 2: Cessation of Extension - 91°C @ 1s⁻¹



Part 2: Cessation of Extension - 91°C @ 1s⁻¹

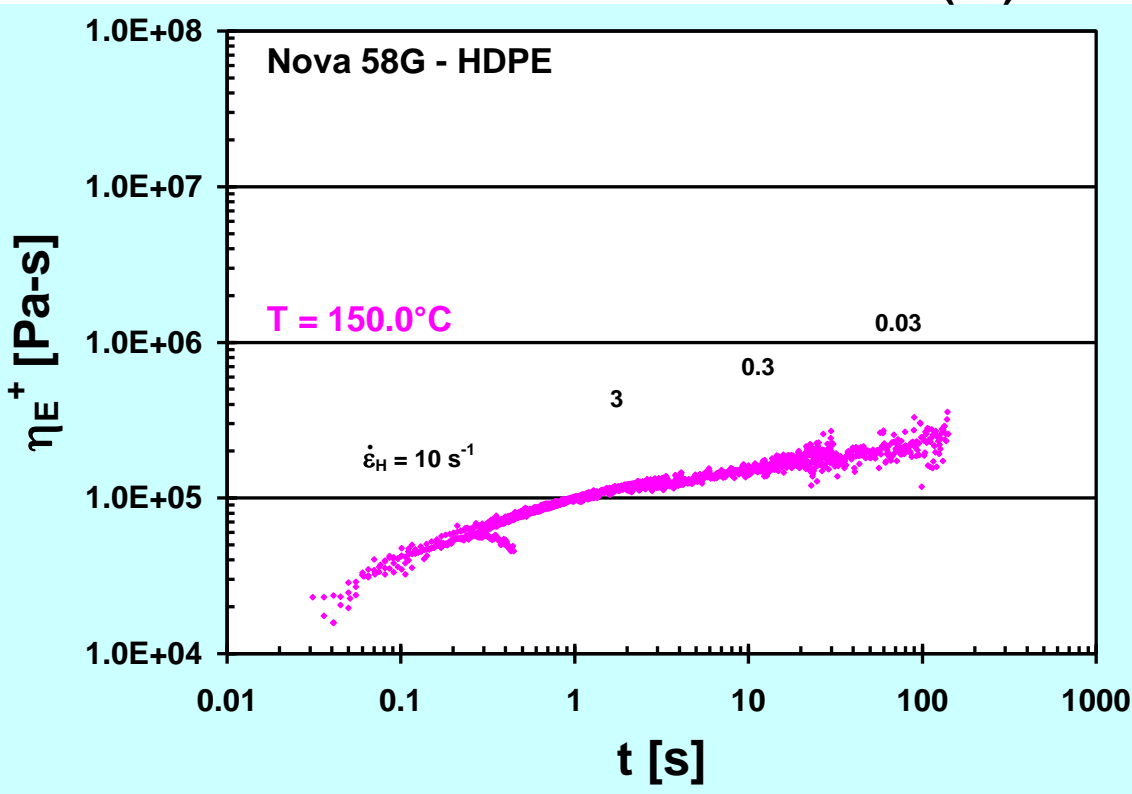
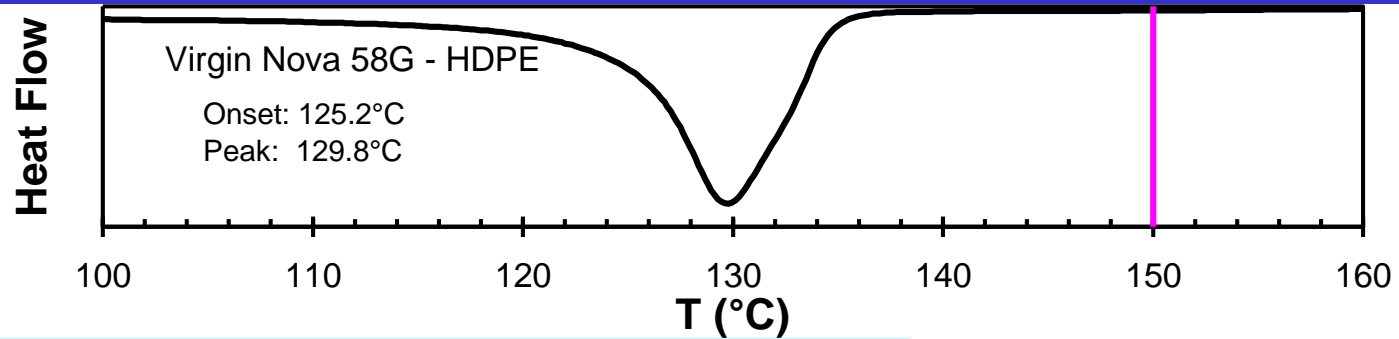


Part 2: Melt Flow Birefringence with the SER

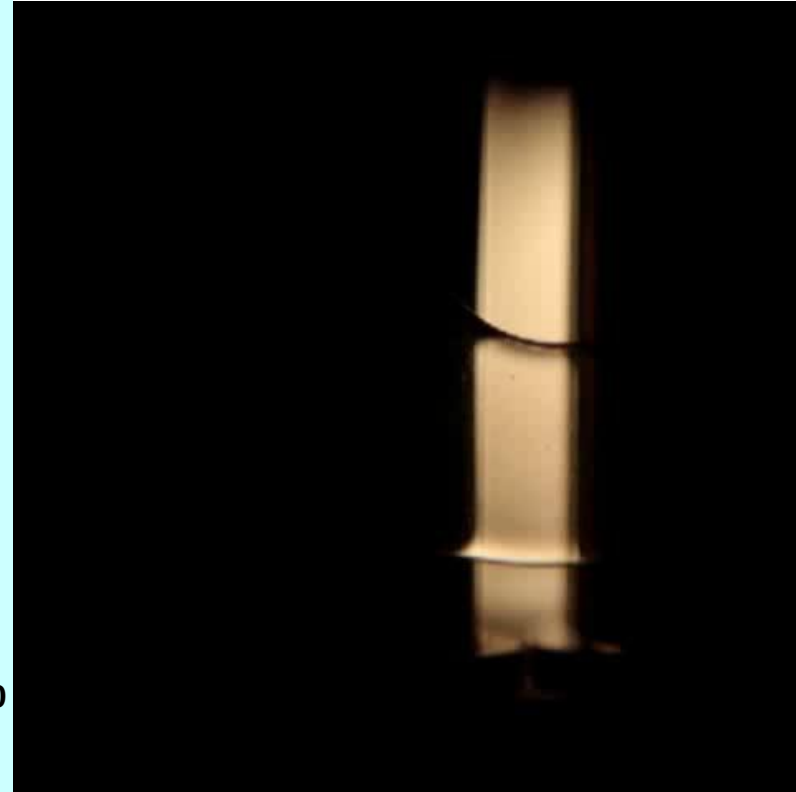
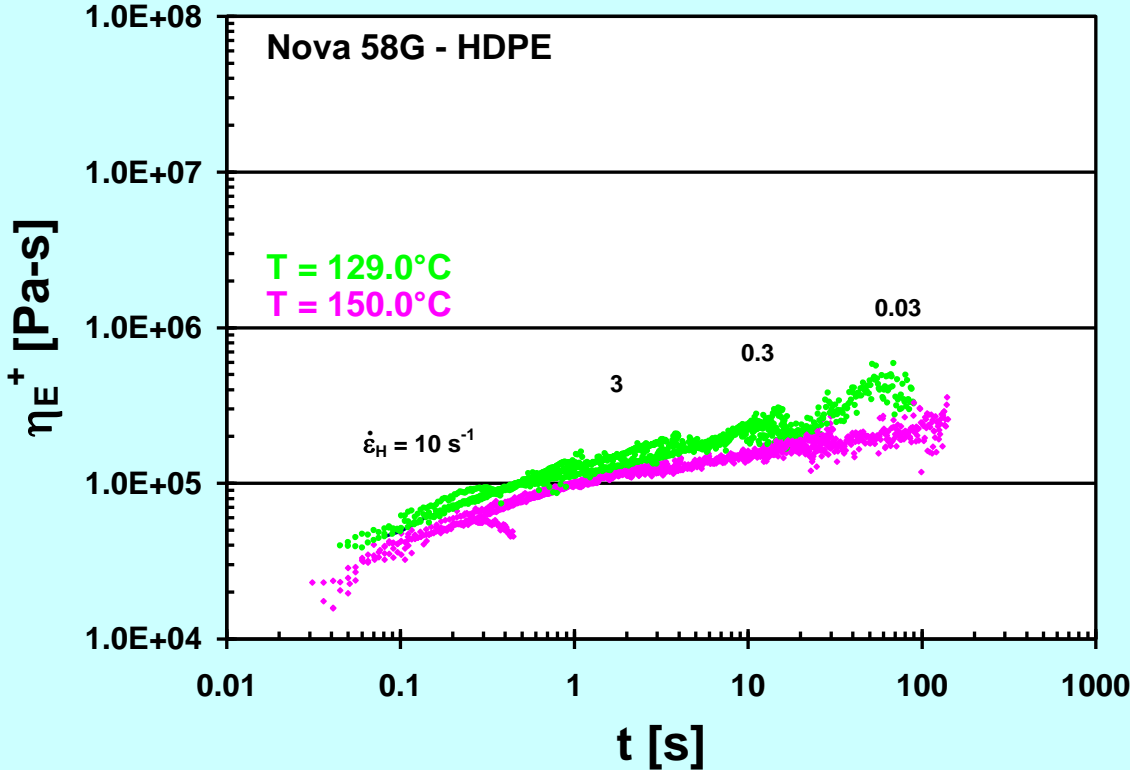
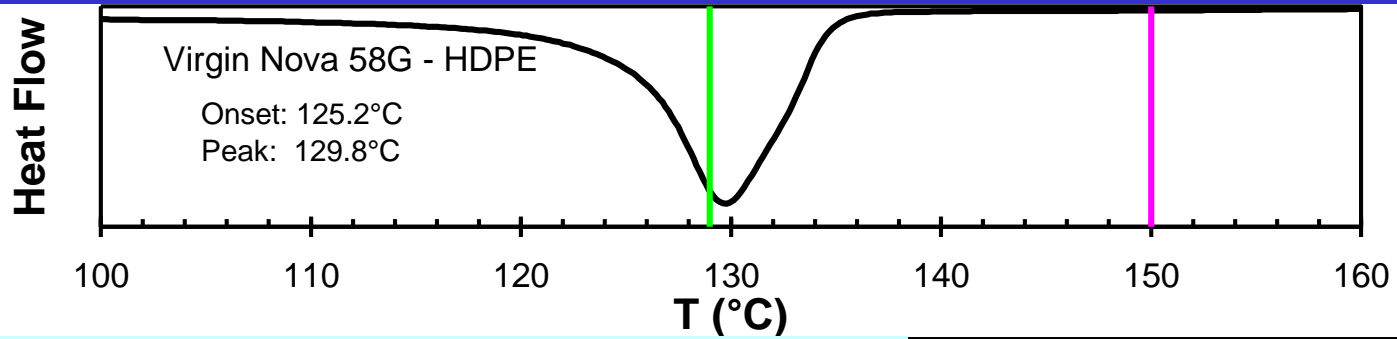


- Because the deformation remains in a fixed plane and in a well-defined stretch zone, flow birefringence measurements can easily be performed with the SER

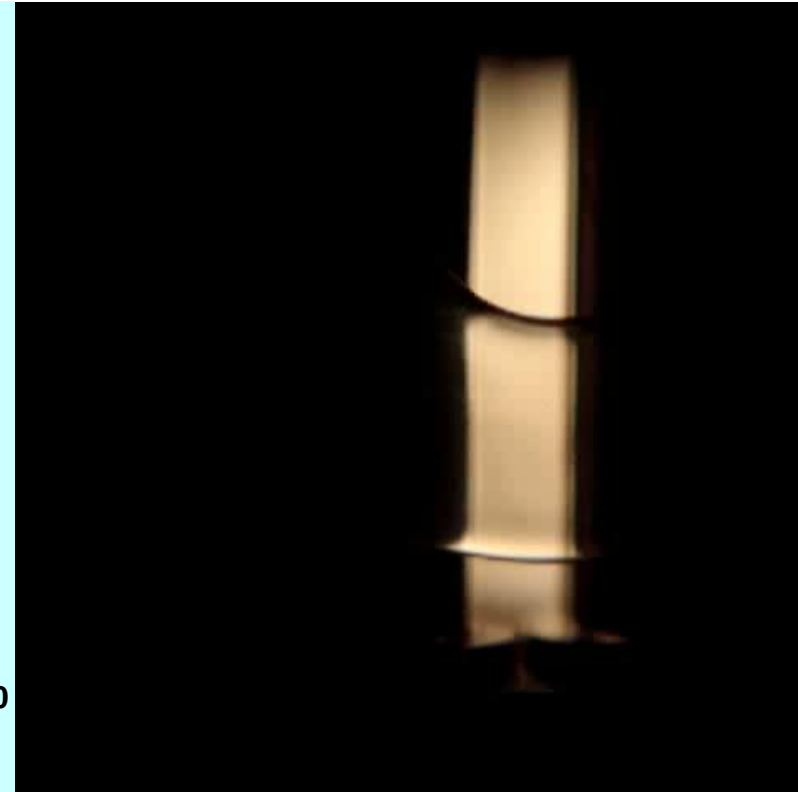
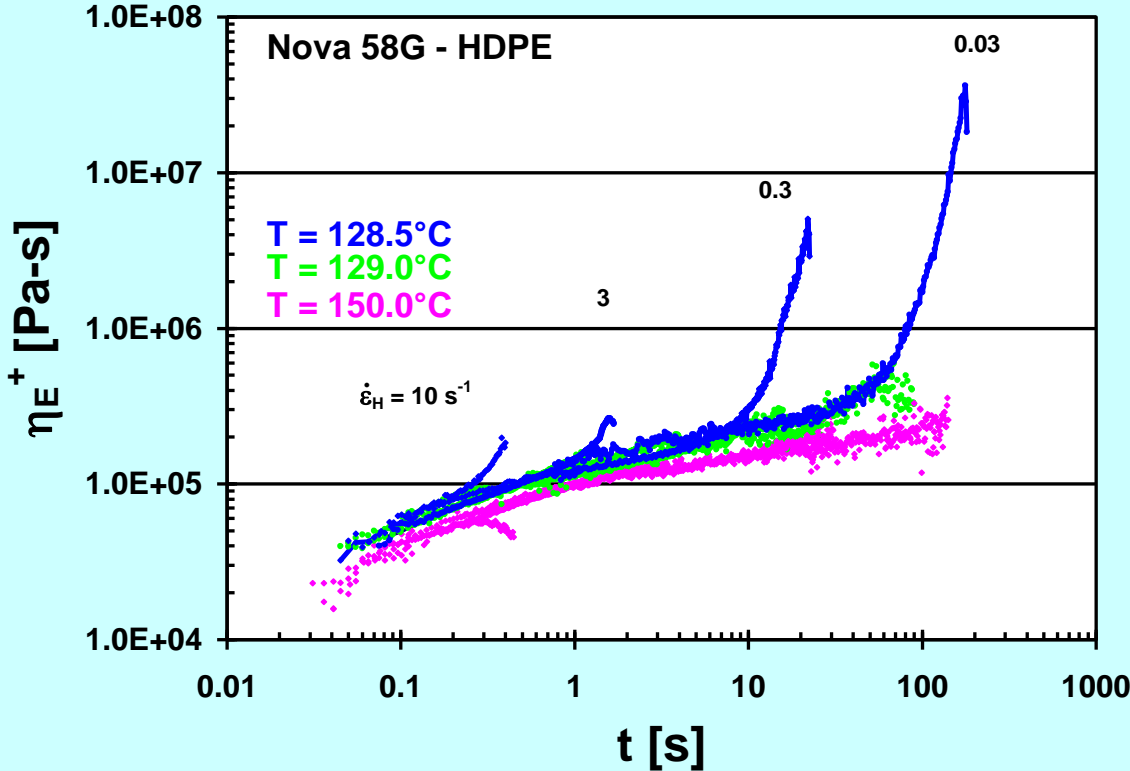
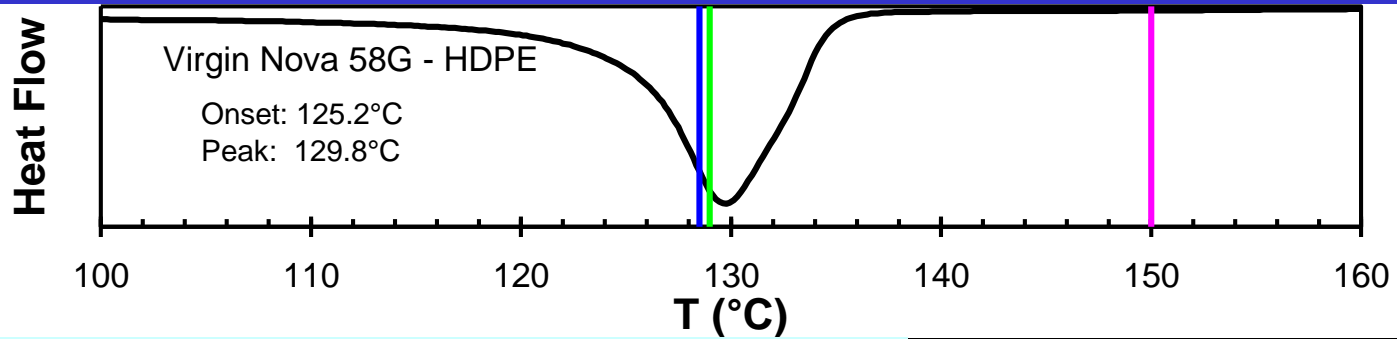
Part 2: Tensile Stress Growth - HDPE



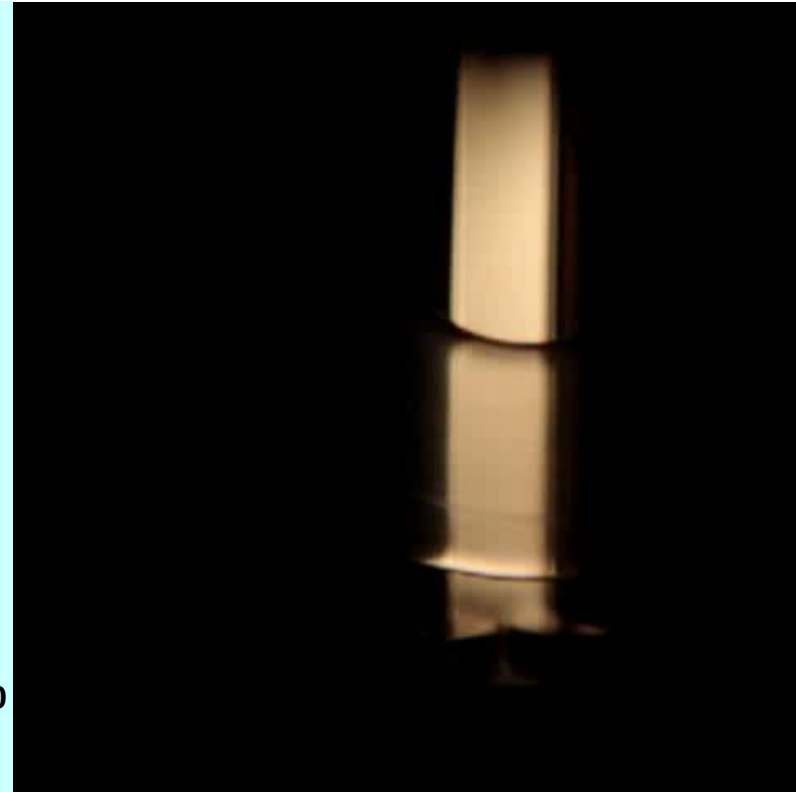
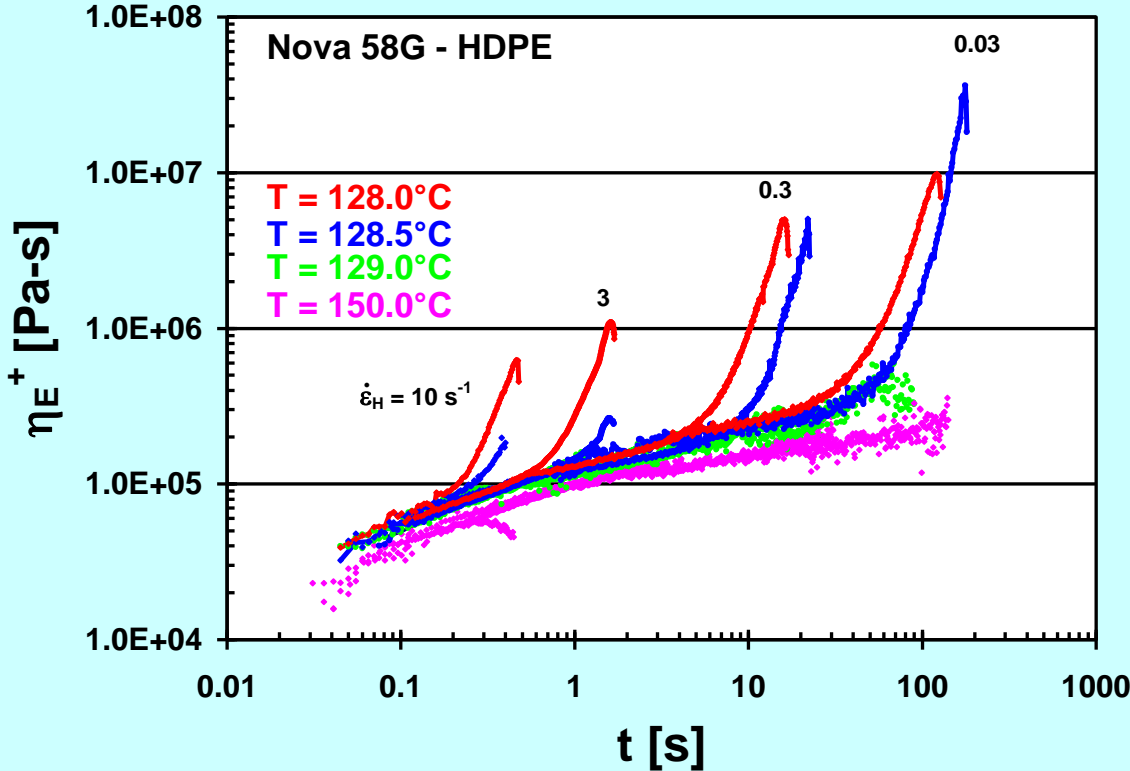
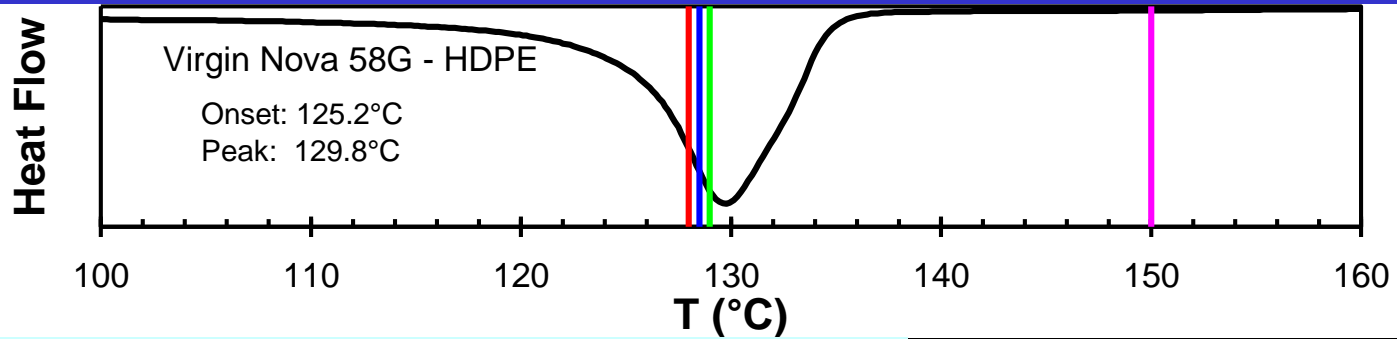
Part 2: Tensile Stress Growth - HDPE



Part 2: Tensile Stress Growth - HDPE

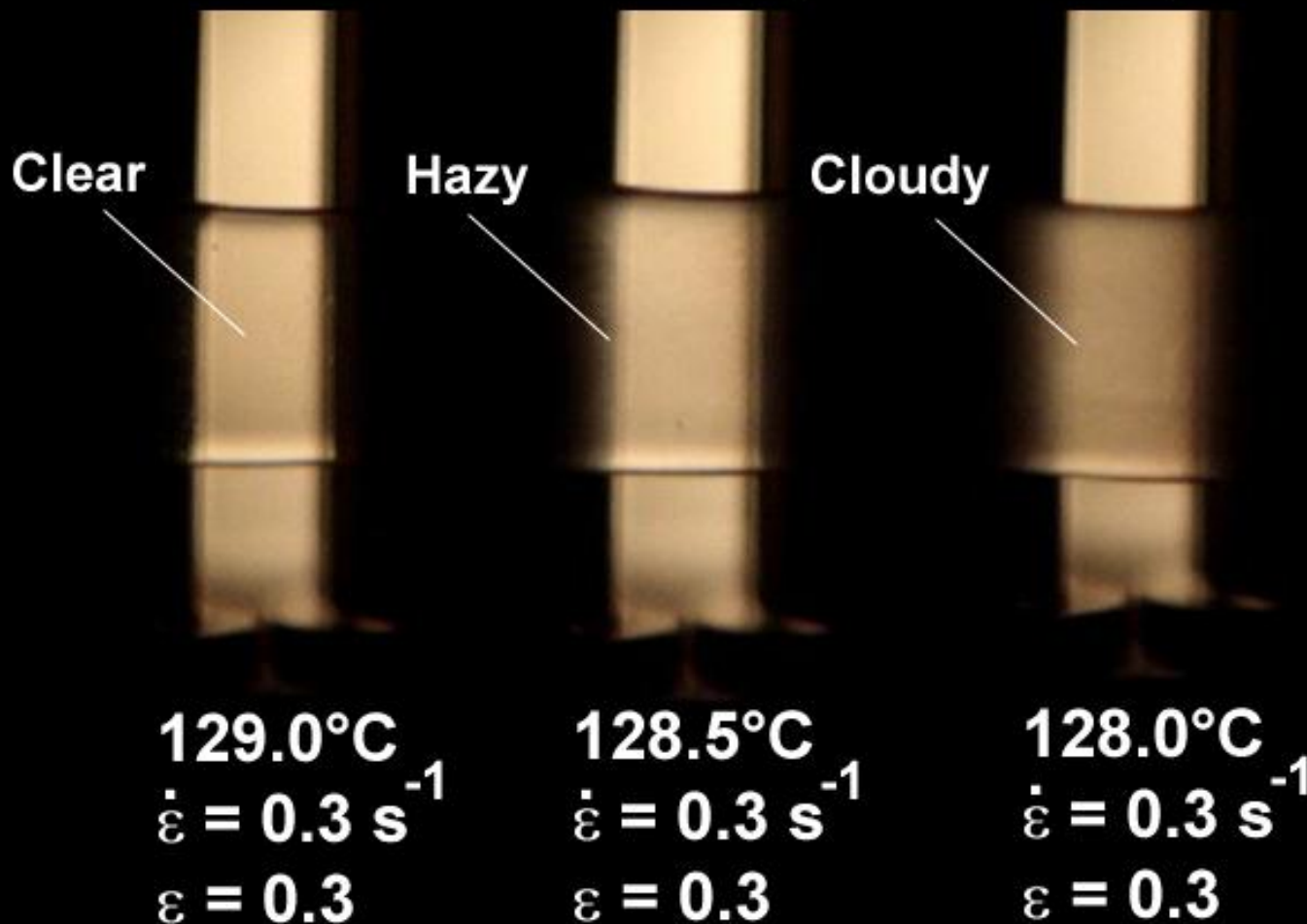


Part 2: Tensile Stress Growth - HDPE

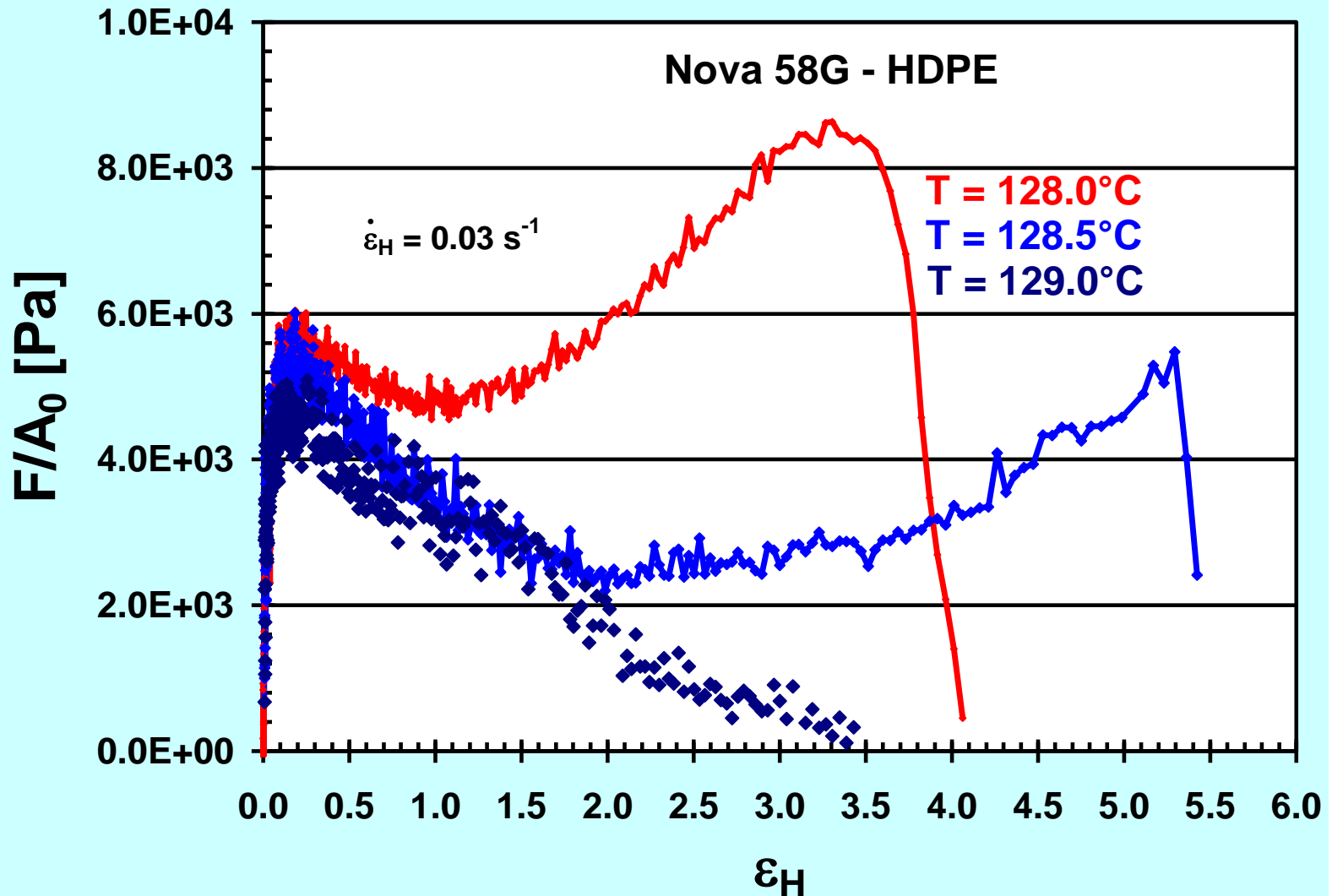


Part 2: Tensile Stress Growth - HDPE

HDPE Melt / FIC Birefringence Comparison



Part 2: Tensile Stress - HDPE



Case Study 3: Mechanism of Melt Fracture Suppression with BN Additive

- Melt fracture is a problem common in the polymer processing industry in which beyond a certain melt throughput extrudate distortion appears



Sharkskin (SS): small periodic distortions appearing on the surface upon exiting the die

(unique to linear polymers - *LLDPE*, *HDPE*)

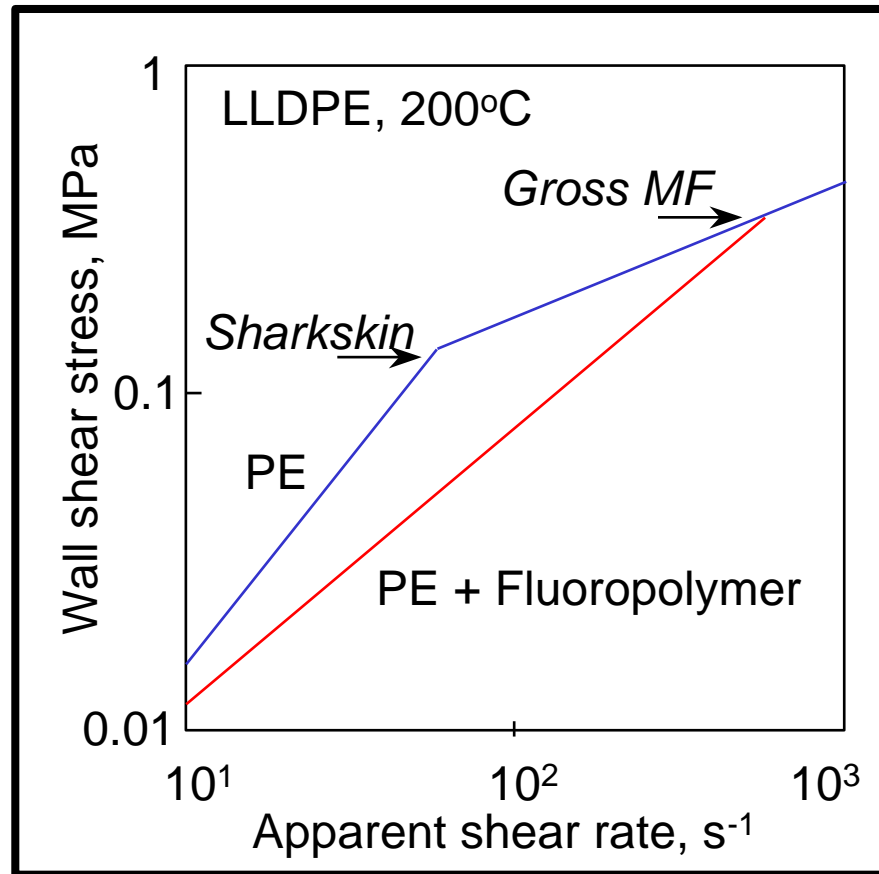


Gross melt fracture (GMF): severe irregular distortions in extrudate appearance

(common with many polymers)



Case Study 3: Processing Aids

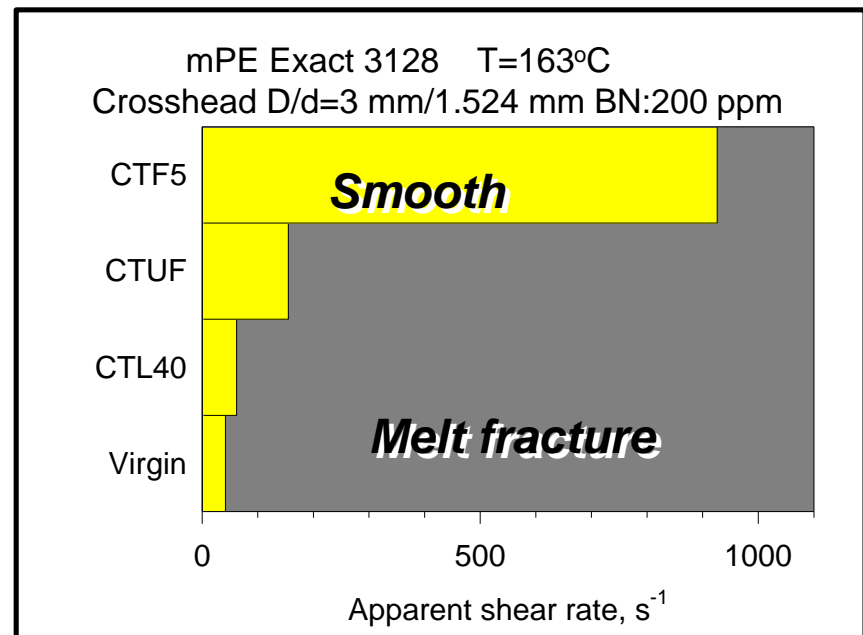
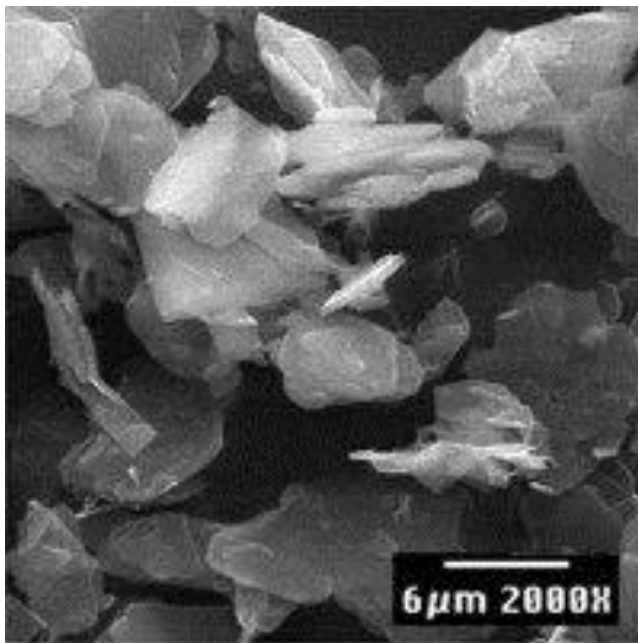


- Although processing aids such as fluoropolymer additives can eliminate sharkskin by coating the die walls and promoting slip, they have no effect on the occurrence of gross melt fracture



Case Study 3: Boron Nitride (BN)

- Recently certain Boron Nitride (BN) powder additives have been found to be effective in eliminating sharkskin and significantly delaying the onset of GMF, although the mechanism by which this occurs remains uncertain

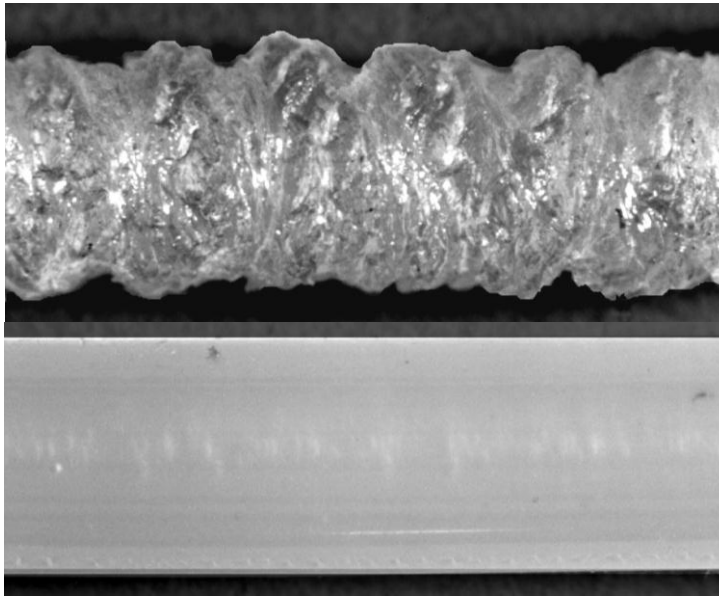


(h-BN: soft, graphite-like ceramic platelet particles)

Case Study 3: Objective

Elucidate the mechanism by which boron nitride powder additives affect the onset of gross melt fracture in commercial linear polyethylenes.

$$\dot{\gamma}_A = 617 \text{ s}^{-1}$$

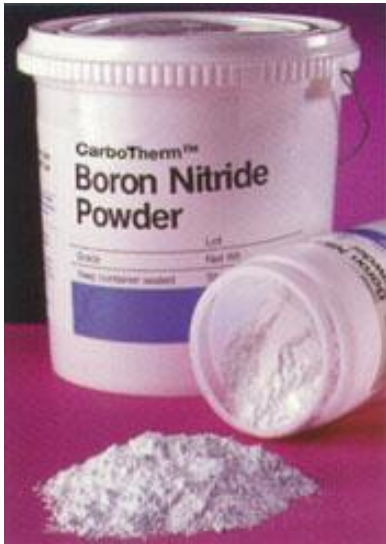


m-LLDPE (Pure)

m-LLDPE + 0.1% BN



Case Study 3: Experimental



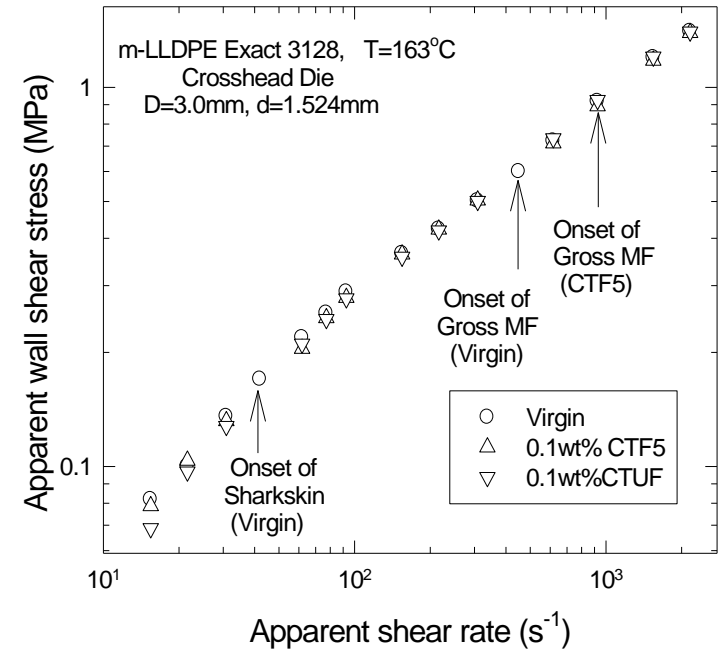
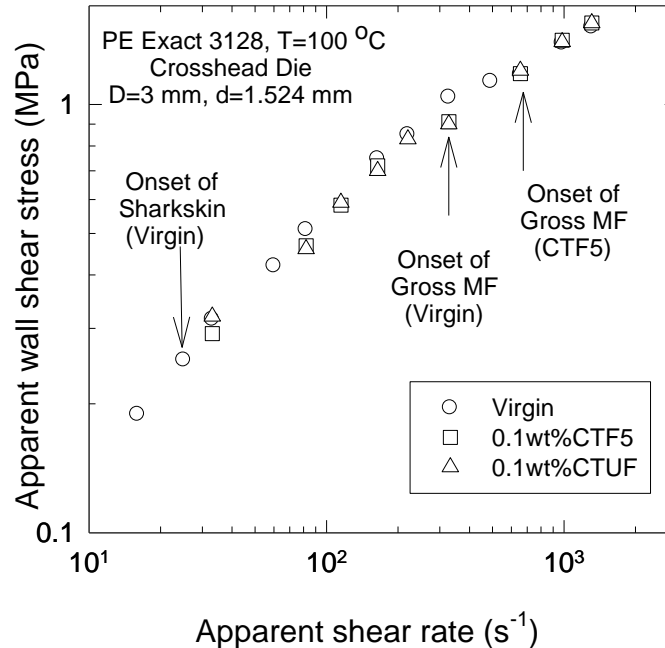
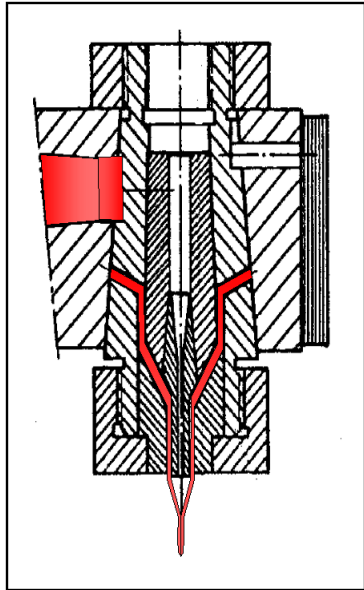
- BN Powders from Saint-Gobain Advanced Ceramics
(5-20 μm particle size) compounded at 0.1wt. %
 - ◆ CarboTherm™ CTF5 (SE: 47.1 [11] mJ/m^2)
 - ◆ CarboTherm™ CTUF (SE: 63.4 [27] mJ/m^2)

■ Polymers

- ◆ ExxonMobil Exact 3128 (film grade m-LLDPE, MFI = 1.2)
- ◆ ExxonMobil Exceed 143 (film grade m-LLDPE, MFI = 1)
- ◆ BP Chemicals PF-Y821-BP (film grade ZN LLDPE, MFI = 0.8)



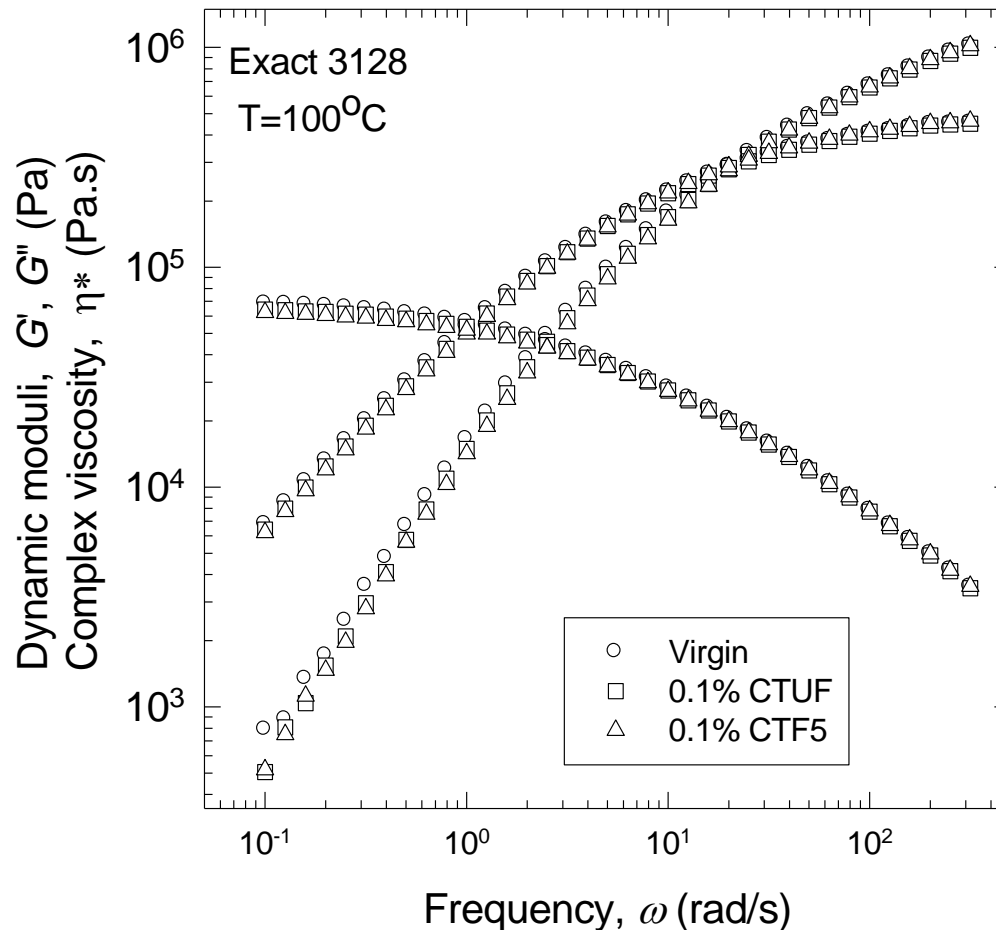
Case Study 3: Exact 3128 Processing Behavior



| | Critical Shear Rates for the Onset of: | | | |
|------------------------|--|-----|-------|-----|
| | 100°C | | 163°C | |
| | SS | GMF | SS | GMF |
| Exact 3128 (Virgin) | 25 | 327 | 42 | 450 |
| Exact 3128 + 0.1% CTUF | 80 | 650 | 150 | 920 |
| Exact 3128 + 0.1% CTF5 | - | 655 | - | 928 |

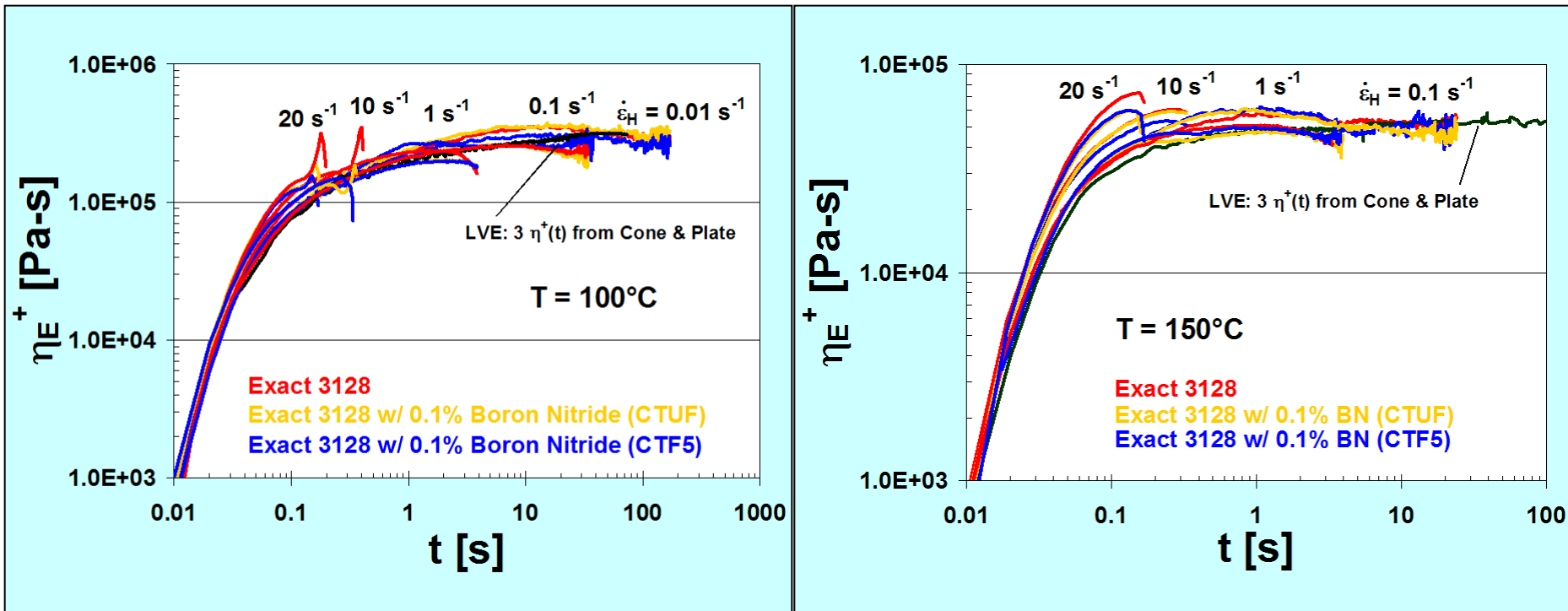
Despite displaying almost identical flow curves, the presence and type of BN appears to play a large role in melt fracture behavior

Case Study 3: SAOS Exact 3128



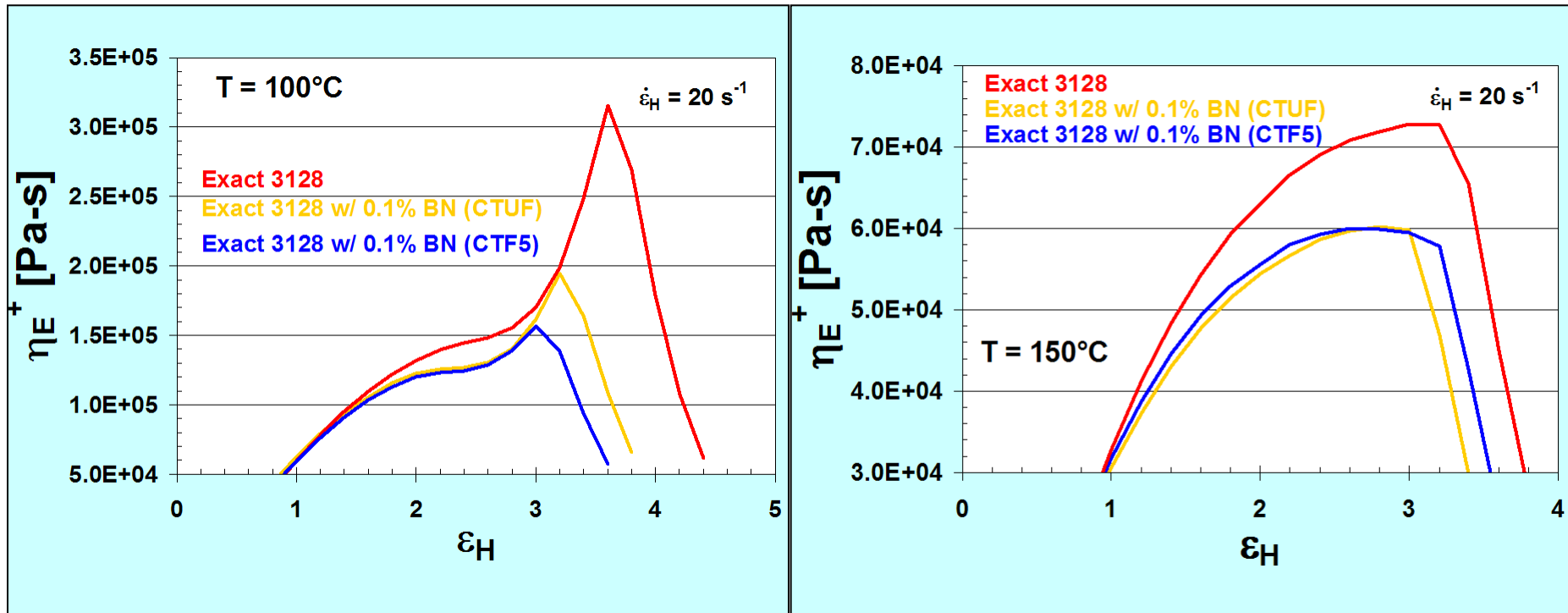
LVE results from SAOS are incapable of revealing any unique information about the effect of BN on polymer behavior

Case Study 3: Tensile Stress Growth - Exact3128



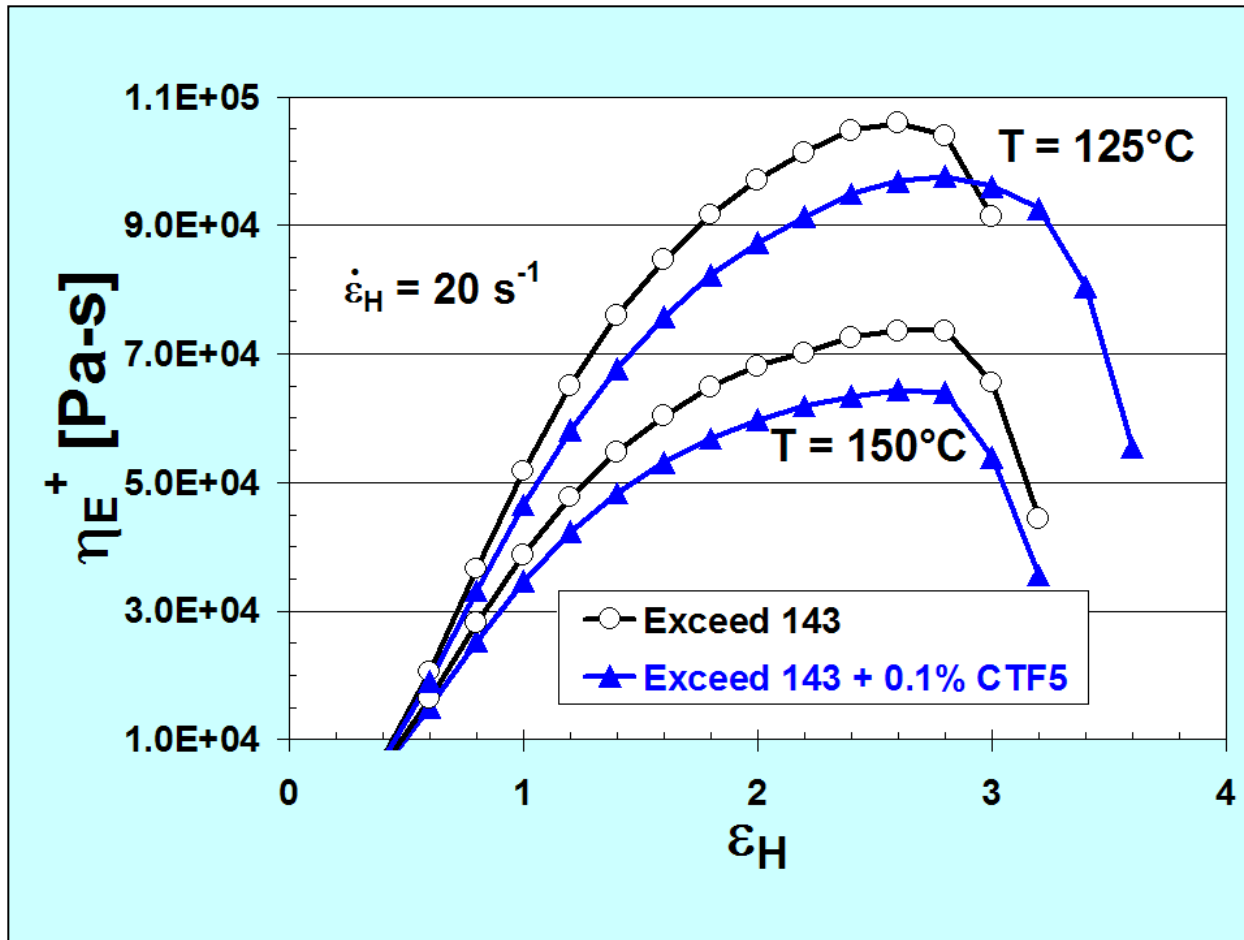
- As the rate of extension increases, the sample rupture transitions from a ductile to a brittle-type mode of failure, coinciding with rubbery behavior at short times
- Only at high extensional flow rates are differences in the polymers clearly evident

Case Study 3: Exact 3128 High-Rate Extensional Flow



- Note that the BN-filled polymers exhibit subdued stress growth and peak stresses at high extensional rates
- These results suggest that the presence of BN serves as an energy dissipater/plasticizer that inhibits the elastic/rubber-like behavior of the m-LLDPE polymer at large deformations and rates

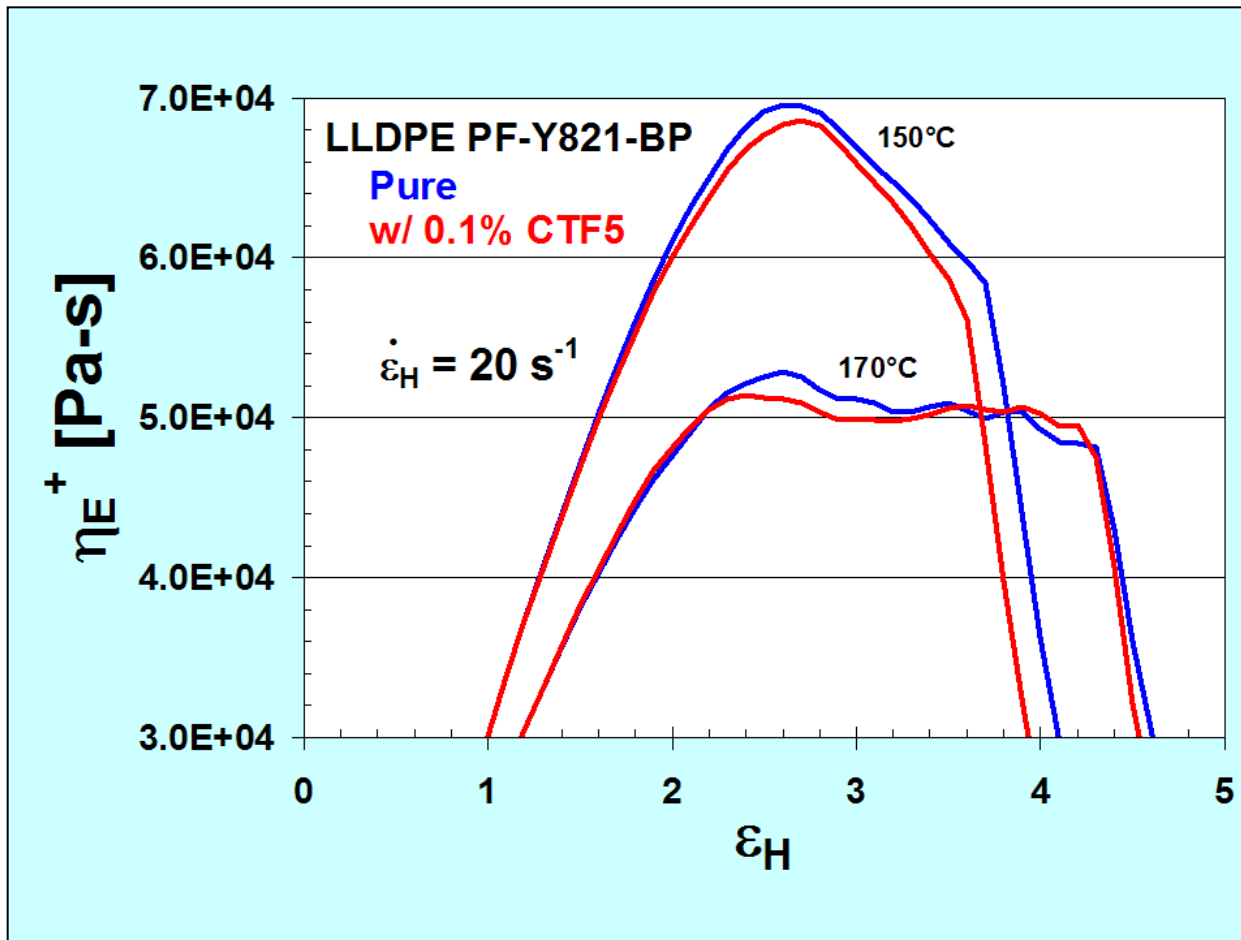
Case Study 3: Exceed 143 High-Rate Extensional Flow



- The presence of BN appears to have a similar energy dissipation effect on Exceed 143 (m-LLDPE)

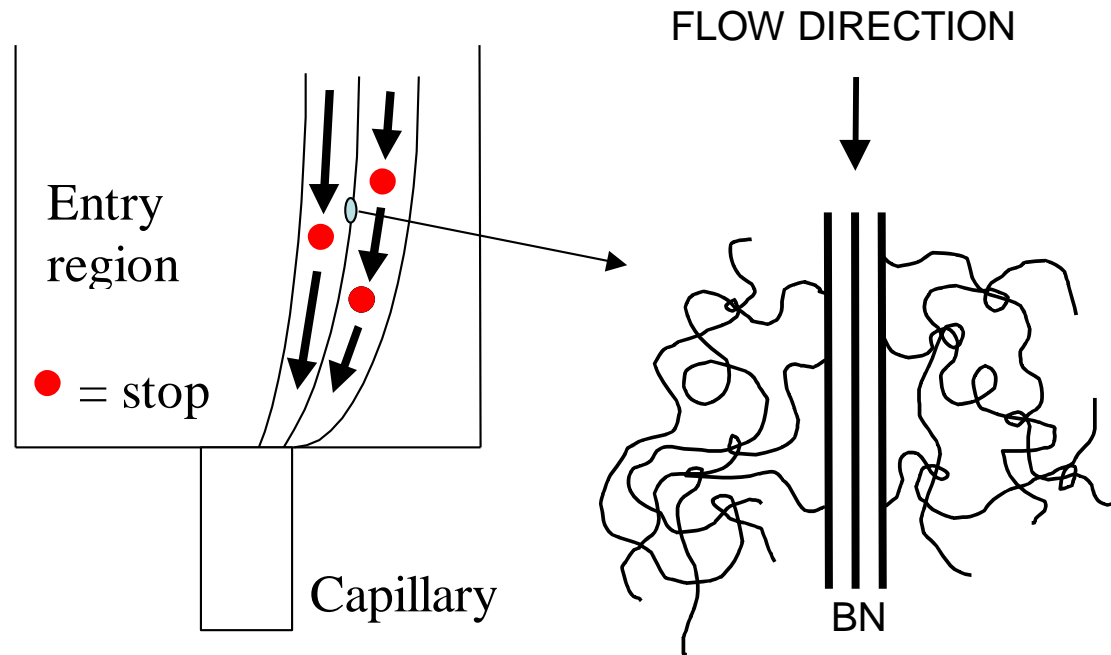


Case Study 3: PF-Y821-BP High-Rate Extensional Flow



- The presence of BN also has a similar energy dissipation effect on PF-Y821-BP (ZN-type LLDPE)

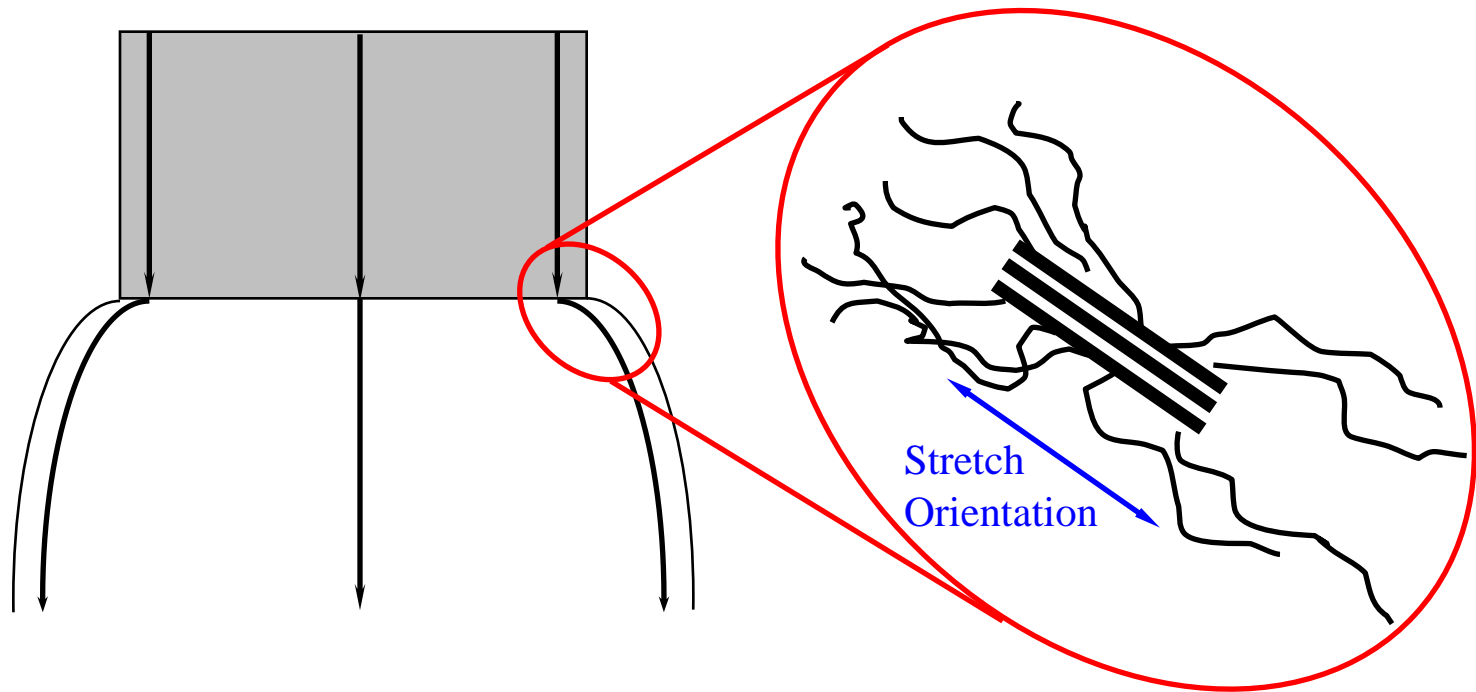
Case Study 3: Mechanism of GMF Suppression by BN



- The large platelet structure of the BN particles allow for a significant number of polymer adsorption sites on the BN surface
- At high rates and deformations in the die entry region, the energy normally borne by the polymer chain backbone is dissipated via the reconfiguration/release of polymer chains on the BN surface



Case Study 3: Mechanism of SS Suppression by BN



- Upon exiting the die the polymer chains nearest the skin of the extrudate undergo very large and rapid stretching deformations
- The presence of BN serves as a “plasticizer” for these polymer chains by dissipating the storage of elastic energy via the reconfiguration/release of polymer chains on the BN surface



Case Study 4: Detecting Differences in Polymer Macrostructure - PE

■ Four Commercial Polyethylenes:

- ◆ LD200: Coating Grade LDPE (ExxonMobil), MI = 7.5
- ◆ LL3001.32: Film Grade LLDPE (ExxonMobil), MI = 1.0

Part 1

- ◆ EF606: Film Grade LDPE (Westlake Polymers), MI = 2.2
- ◆ Exact 3128: Film Grade m-LLDPE (ExxonMobil), MFI = 1.2

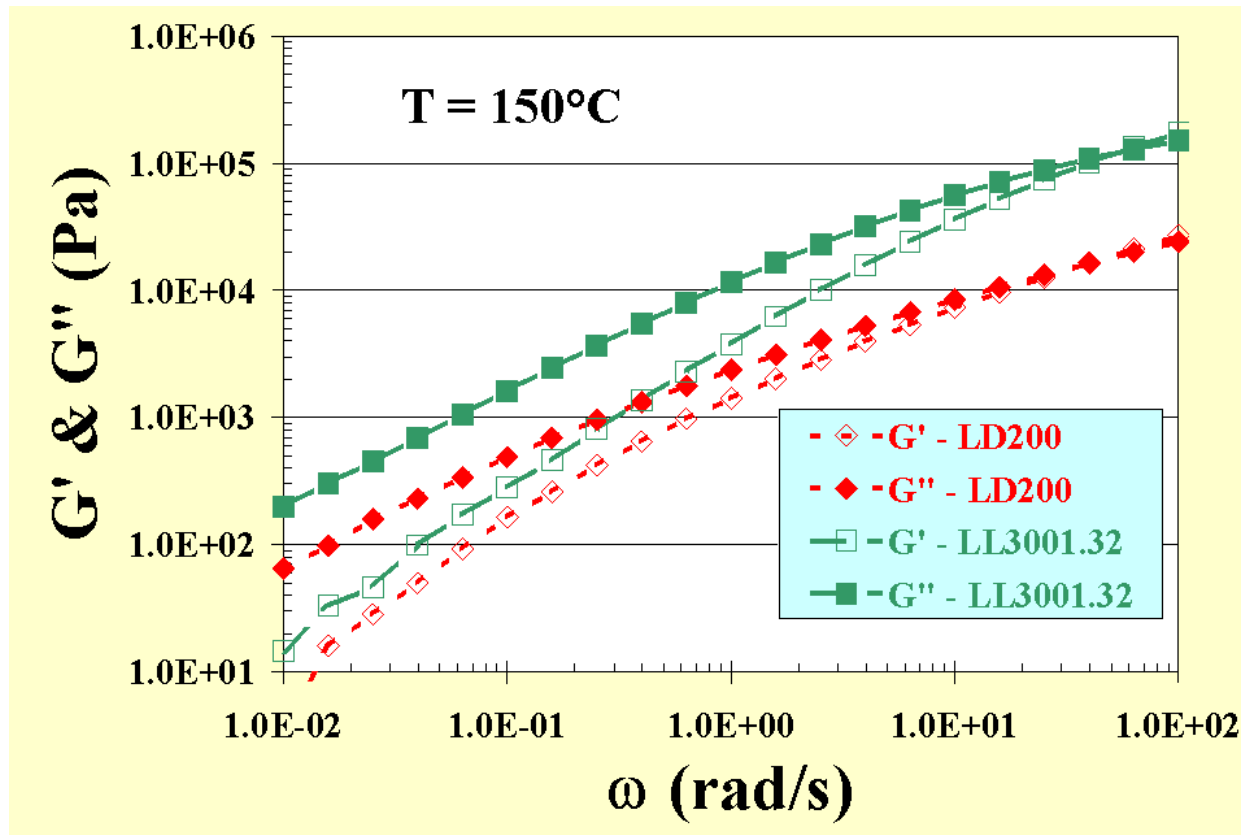
Part 2

■ *Exercise:*

Detect differences in polymer macrostructure between these four commercial polymers without having any specific macrostructural information about them a priori.

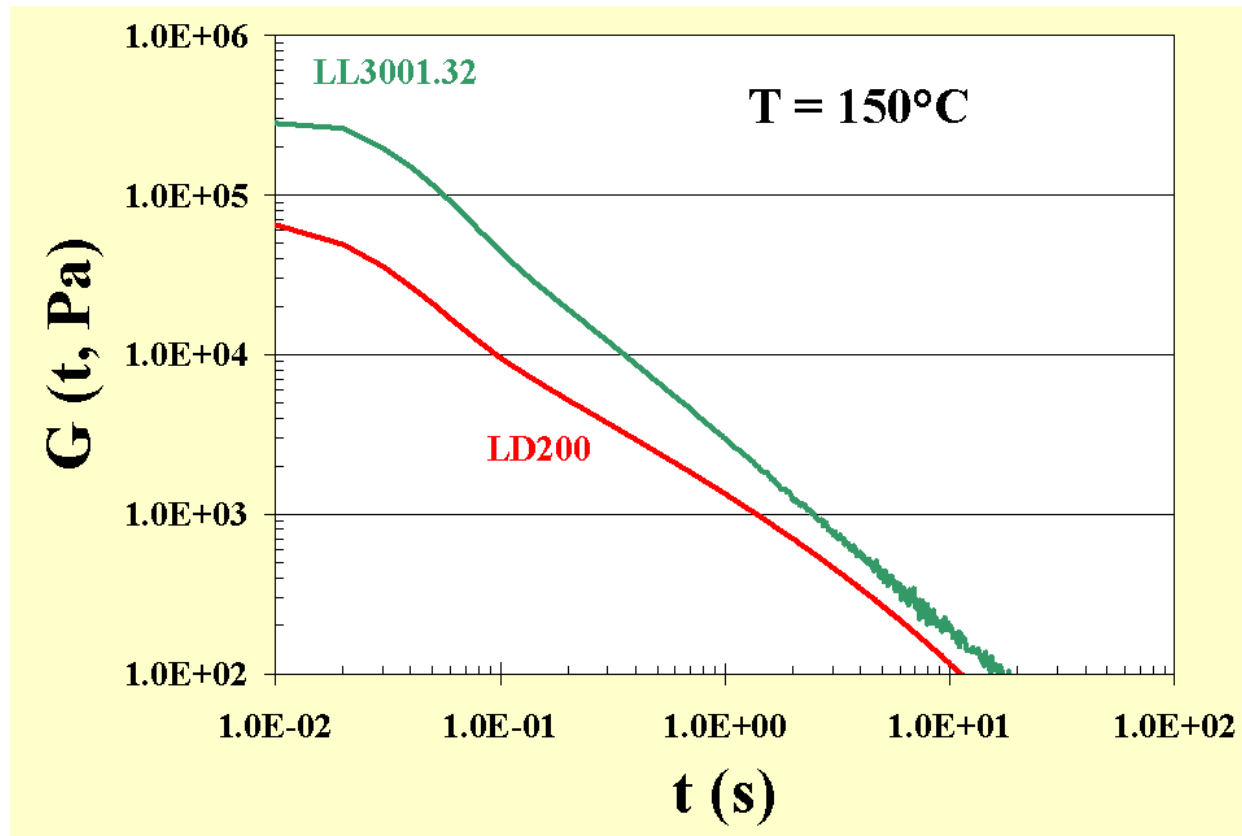


Case Study 4: Part 1 - SAOS Data



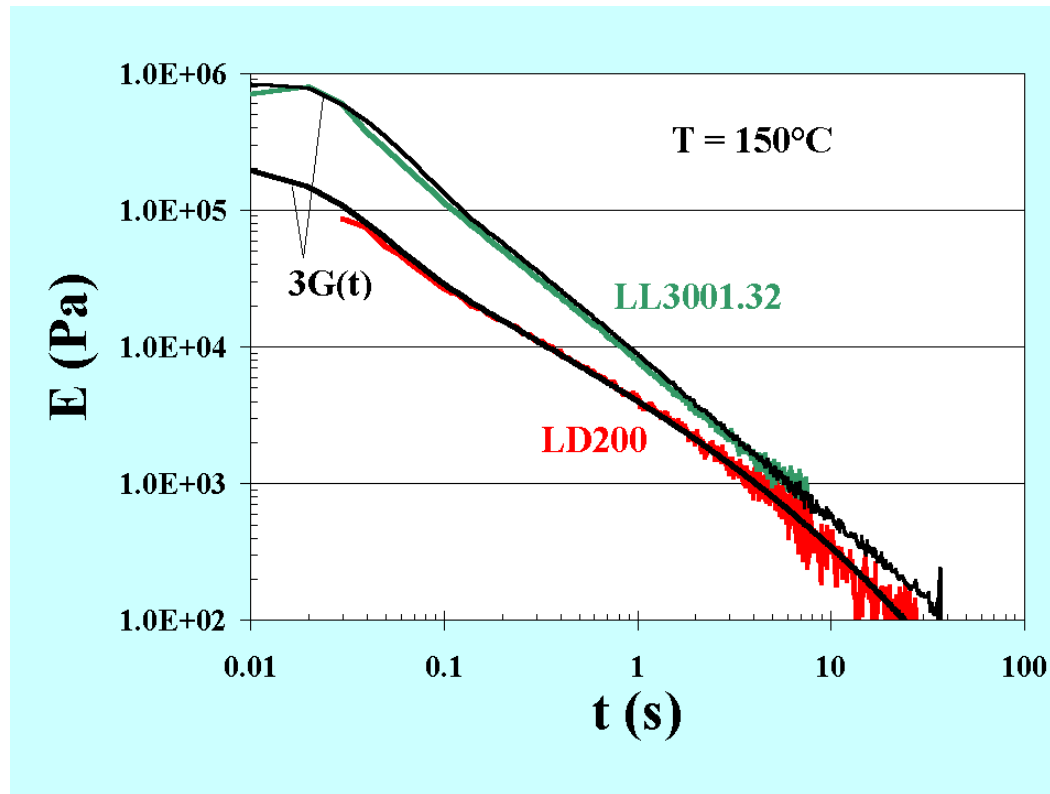
- Despite some notable indications of MW very little can be clearly distinguished between polymer branching and MWD effects from the SAOS data alone.

Case Study 4: Part 1 - LVE Shear Relaxation Data



- Again, despite some notable indications of MW very little can be clearly distinguished between polymer branching and MWD effects from the stress relaxation data alone.

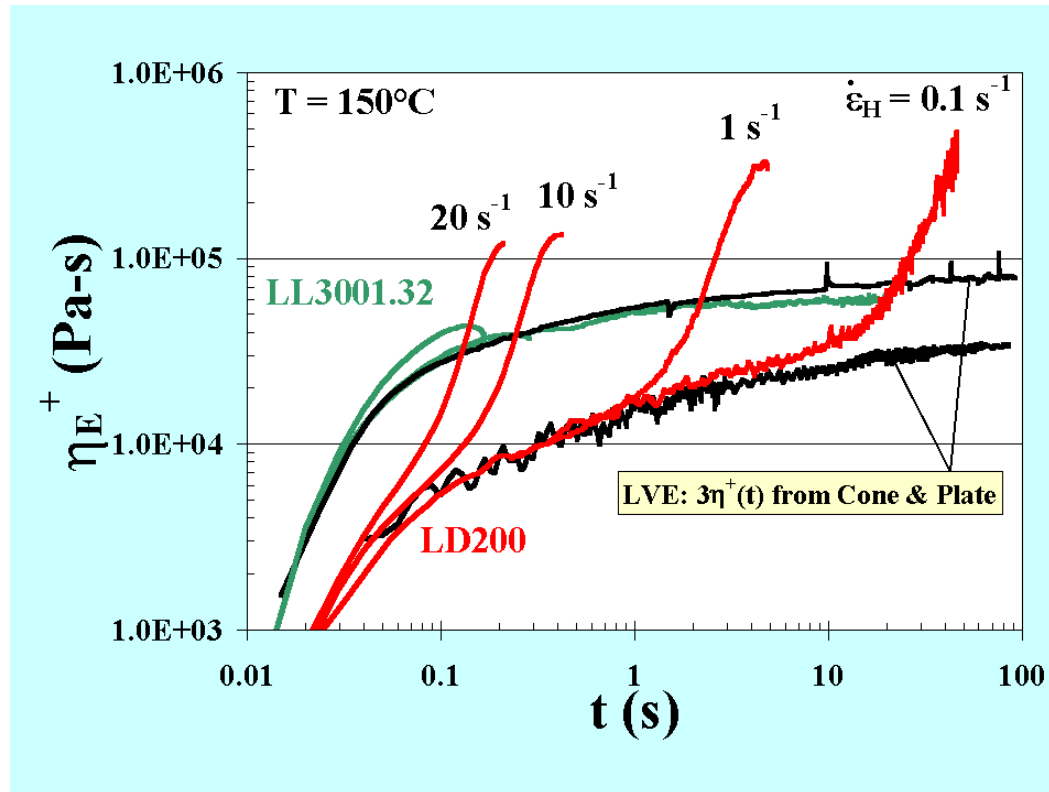
Case Study 4: Part 1 - LVE Extensional Relaxation Data



- Despite excellent agreement between the LVE extension and shear data, again very little can be clearly distinguished between polymer branching and MWD effects from the LVE data alone.



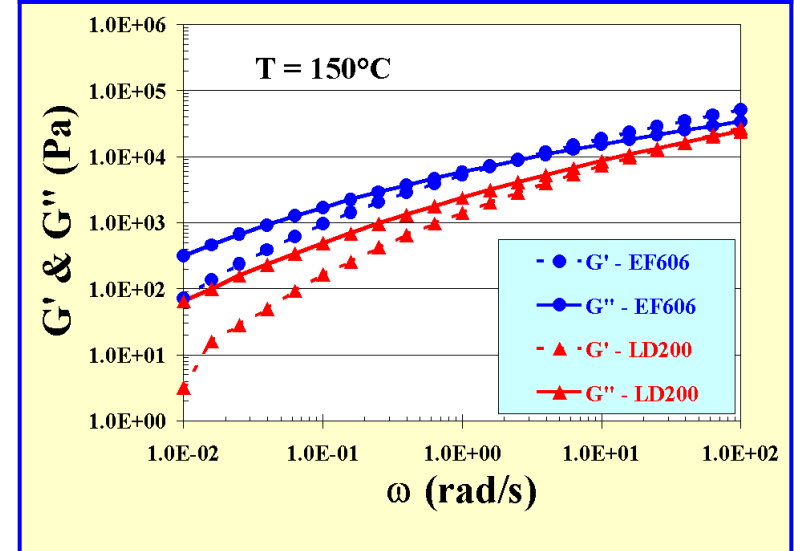
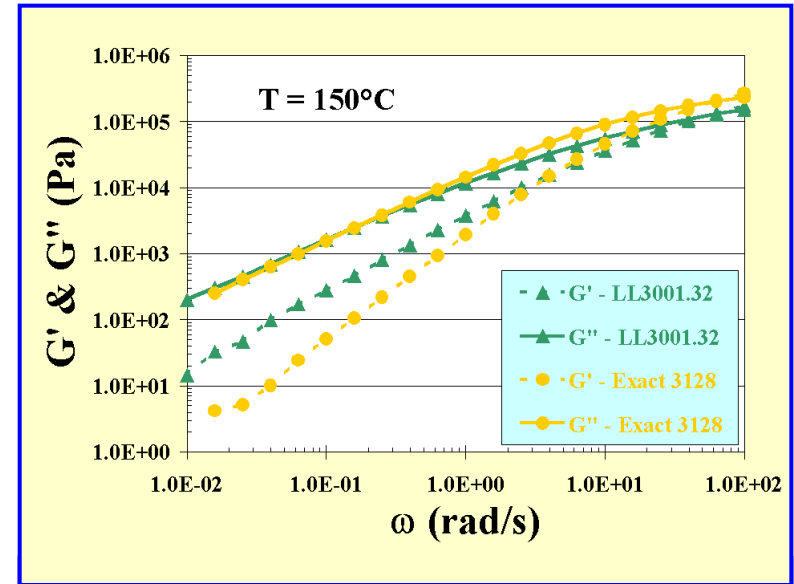
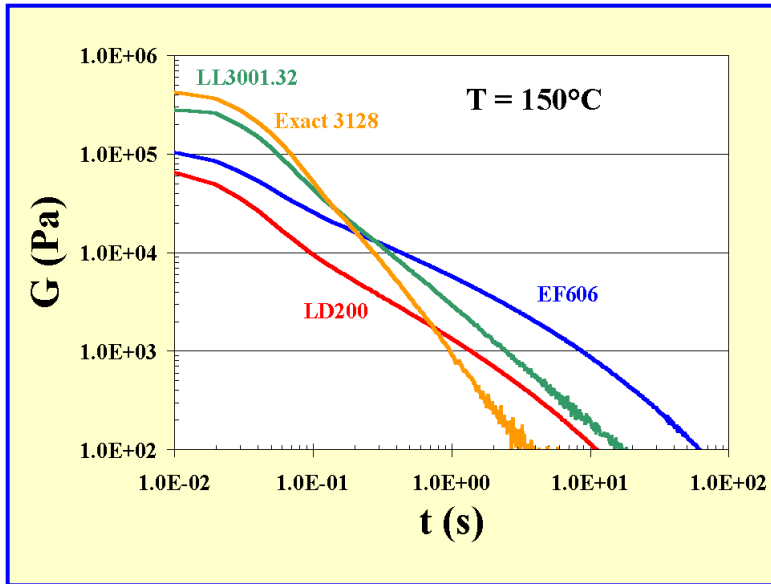
Case Study 4: Part 1 - Tensile Stress Growth



- Note how the tensile stress growth data can clearly distinguish macrostructural features related to branching and MWD - the LDPE exhibits significant strain hardening, behavior consistent with highly branched polymers

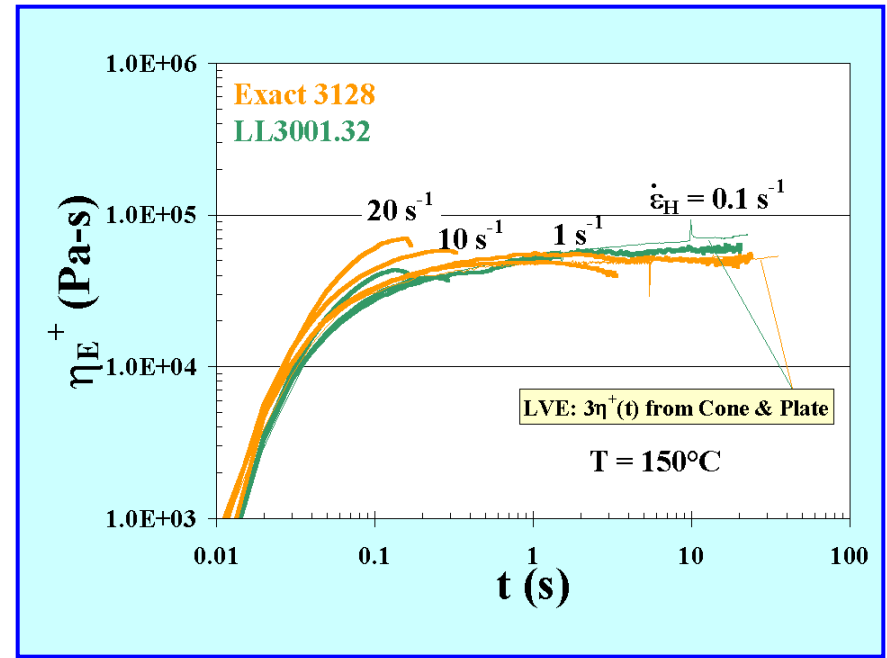
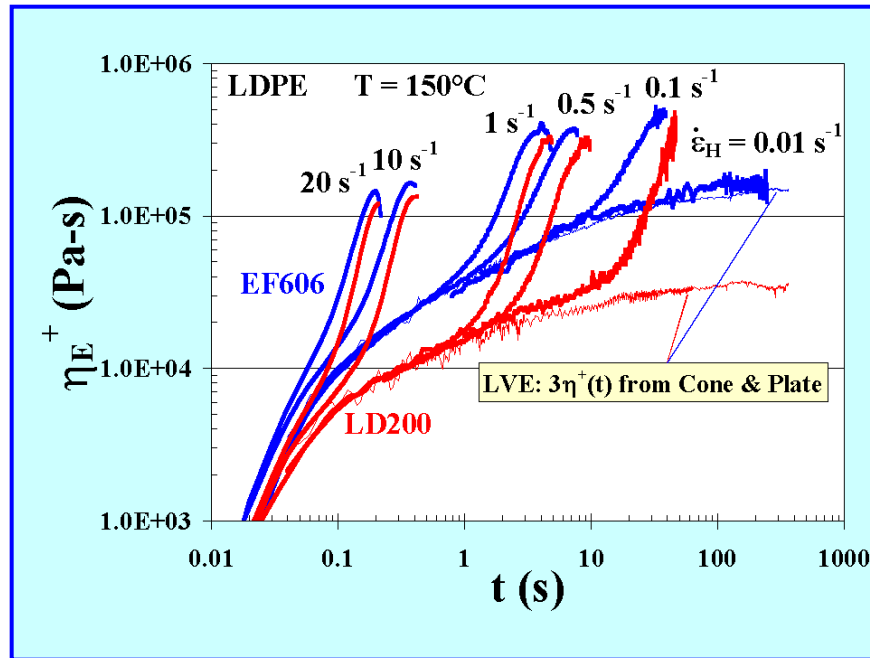


Case Study 4: Part 2 - LVE Data



- Again, despite some indications of MW & MWD very little with regard to macrostructural features such as polymer branching can be concluded from the LVE data alone.

Case Study 4: Part 2 - Tensile Stress Growth



- Note how the tensile stress growth data can clearly differentiate subtle differences in branching as witnessed by the different strain hardening behaviors detected between the two grades of LDPE as well as differences in high-rate melt elasticity with the two LLDPEs

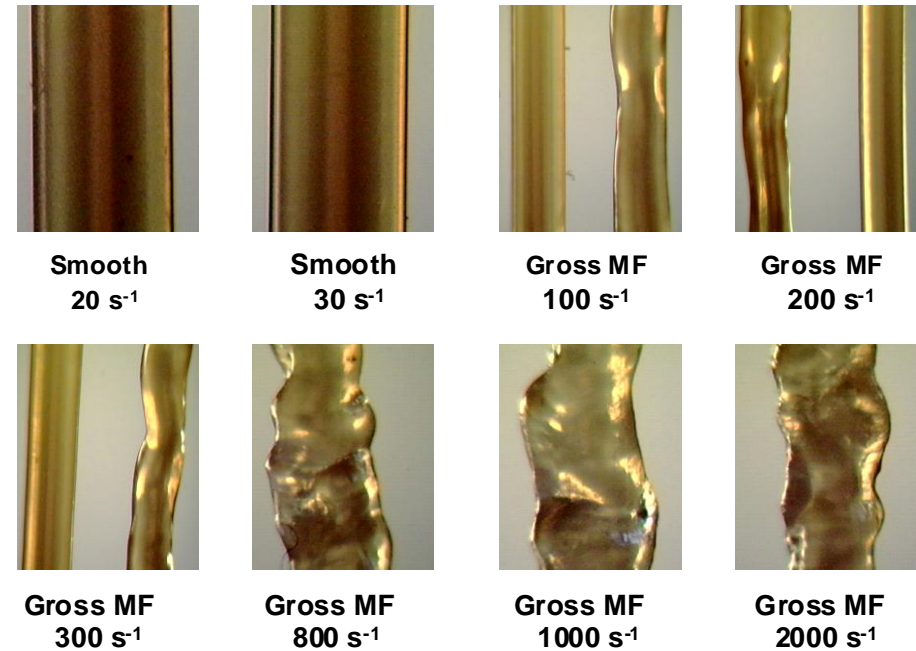
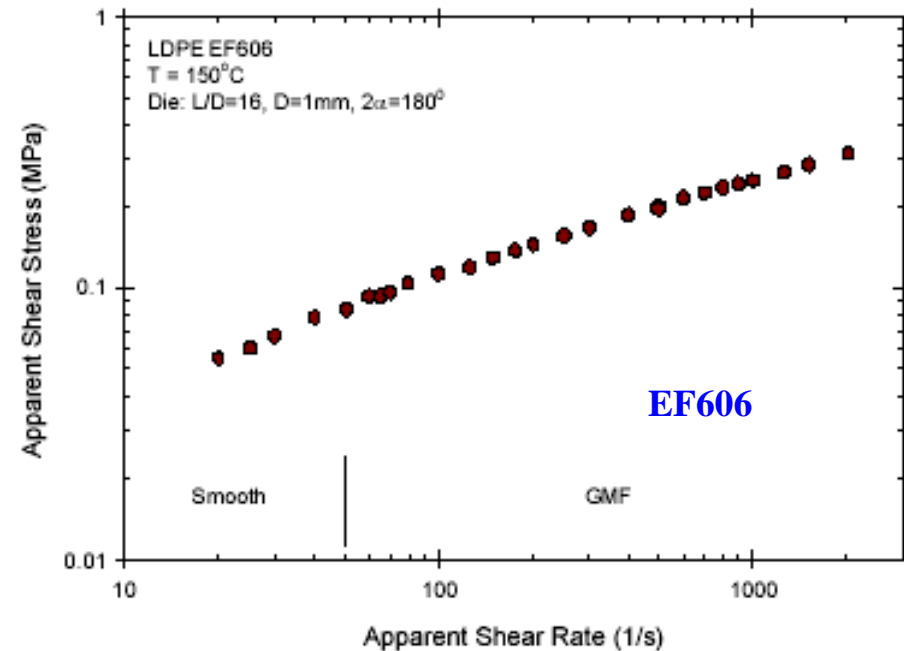
Case Study 5: Elucidating Melt Flow Behavior of Linear & Branched PE

- It is a well known fact that linear polyethylenes exhibits far different processing/extrusion behavior than highly branched polyethylenes
- Despite being investigated extensively for decades some of the fundamental mechanisms for these processing behaviors remain unclear



Case Study 5: Typical LDPE Melt Processing Behavior

LDPE EF606 @ 150°C

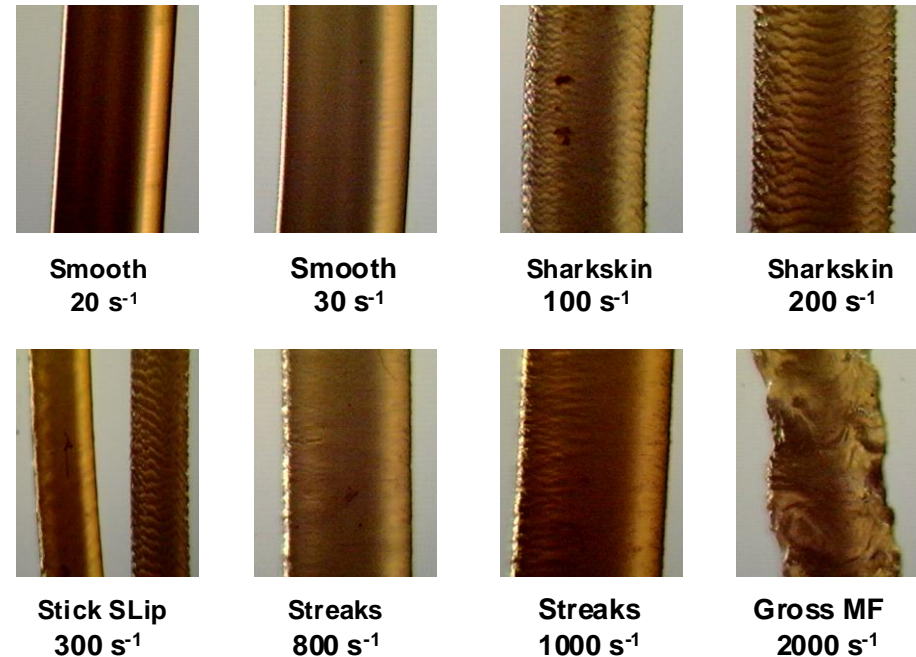
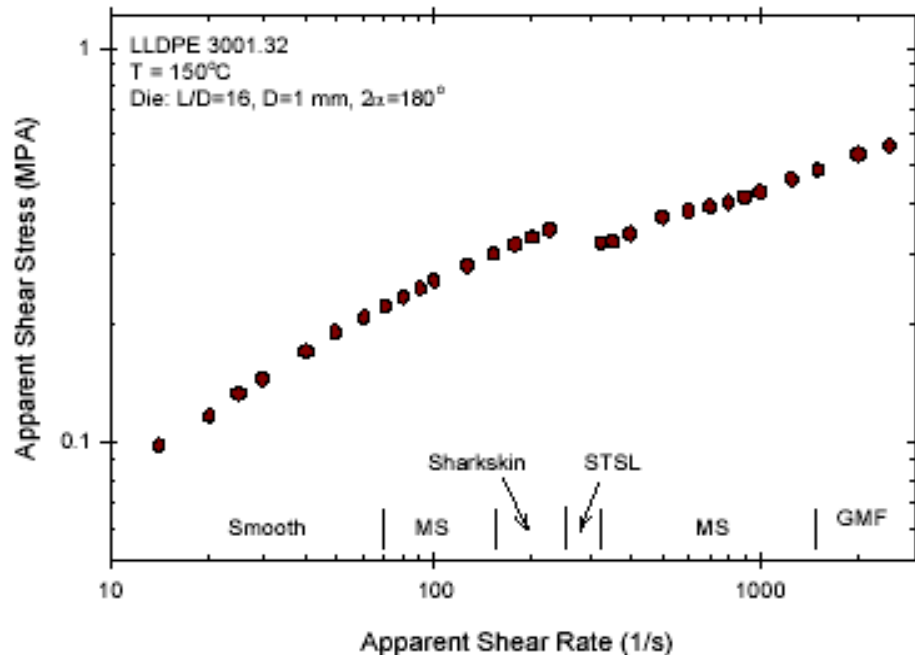


Features of Capillary Extrusion Behavior...

- ◆ *Flow curve*: monotonic increase in shear stress with shear - no discontinuity
- ◆ *Extrudate appearance*: beyond a critical point gross melt fracture (GMF) observed

Case Study 5: Typical LLDPE Melt Processing Behavior

LLDPE LL3001.32 @ 150°C



Features of Capillary Extrusion Behavior...

- ◆ *Flow curve*: at a certain point, notable discontinuity is observed in which the flow becomes unstable over a certain range of flow rates
- ◆ *Extrudate appearance*: extrudate gradually transitions from smooth, to sharkskin, to stick-slip, and eventually gross melt fracture



Case Study 5: Affecting Processing Behavior

Although many efforts have been successful in manipulating processing behavior (*viz a viz* processing aids) many age-old questions remain unanswered:

- ◆ Why does stick-slip flow occur only with linear PE?
- ◆ Why does sharkskin not occur with branched PE?



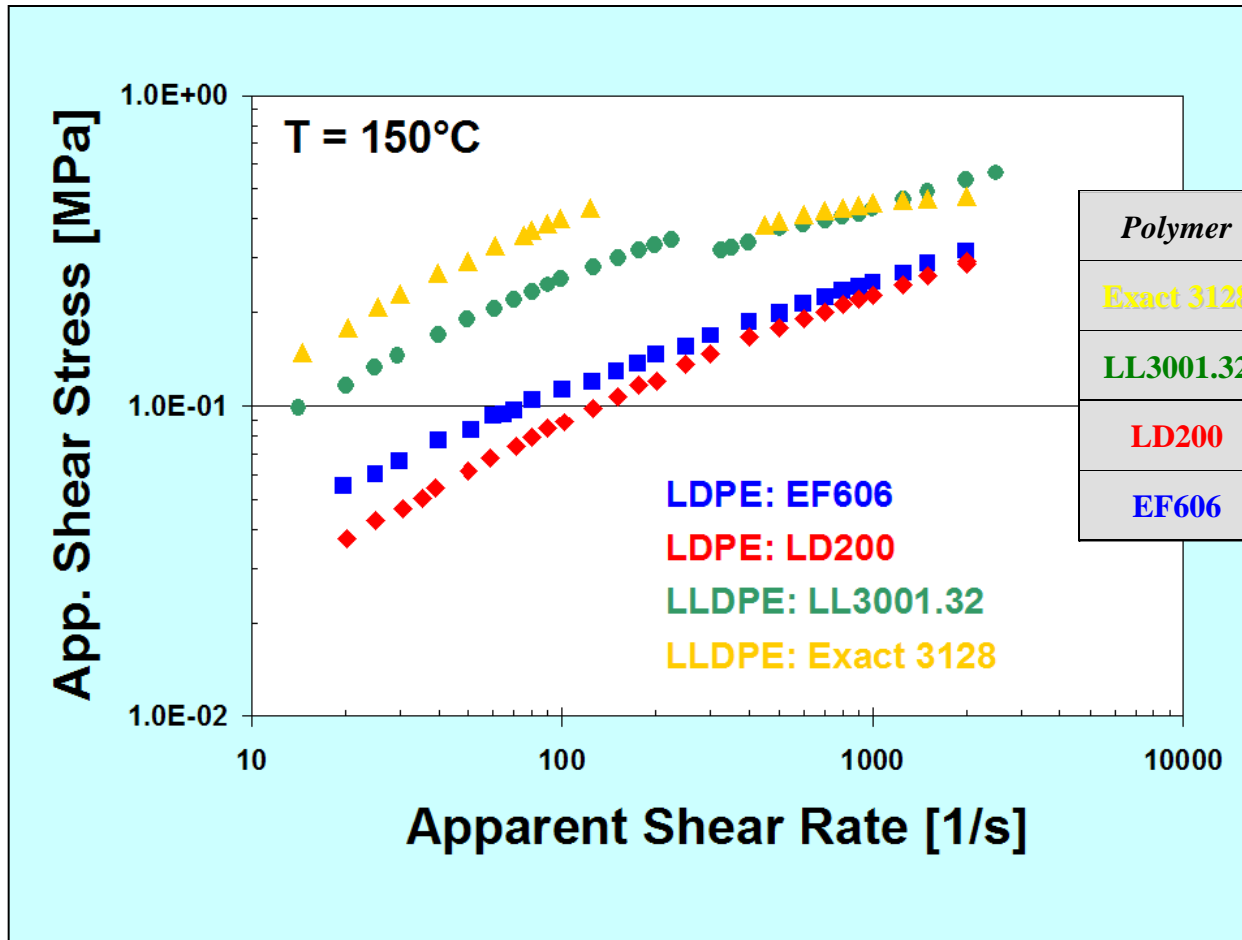
Case Study 5: Experimental

- Four Commercial Polyethylenes:
 - ◆ LD200: Coating Grade LDPE (ExxonMobil), $MI = 7.5$
 - ◆ LL3001.32: Film Grade LLDPE (ExxonMobil), $MI = 1.0$
 - ◆ EF606: Film Grade LDPE (Westlake Polymers), $MI = 2.2$
 - ◆ Exact 3128: Film Grade m-LLDPE (ExxonMobil), $MFI = 1.2$

- Rheological Characterization
 - ◆ Characterize the processing behavior with capillary extrusion
 - ◆ Characterize the extensional flow behavior with the SER
 - ◆ Characterize the dynamic melt adhesion behavior with novel T-peel melt measurements with the SER



Case Study 5: Capillary Extrusion Results



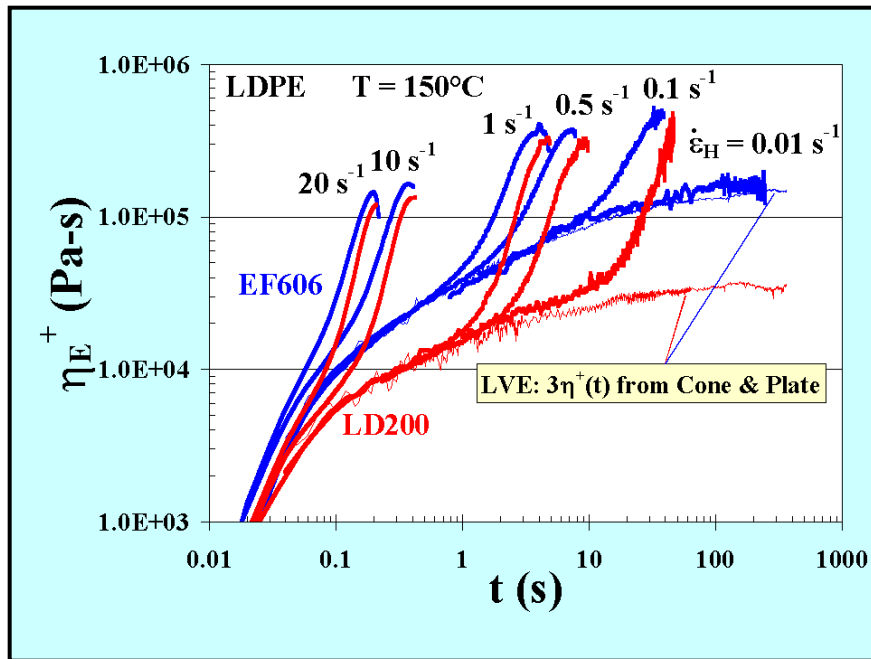
Critical Shear Rates for onset of...

| <i>Polymer</i> | <i>Sharkskin</i> | <i>Stick-slip</i> | <i>Gross MF</i> |
|----------------|------------------|-------------------|-----------------|
| Exact 3128 | 20 | 120 | 420 |
| LL3001.32 | 70 | 240 | 1400 |
| LD200 | - | - | 270 |
| EF606 | - | - | 50 |

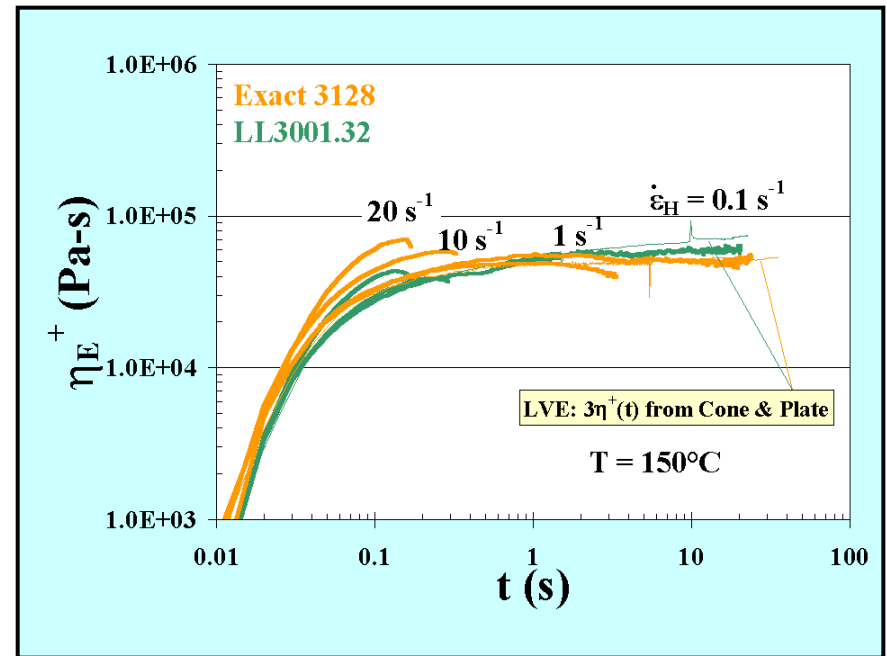
- All four polymers exhibit uniquely different extrusion behavior



Case Study 5: Tensile Stress Growth Results



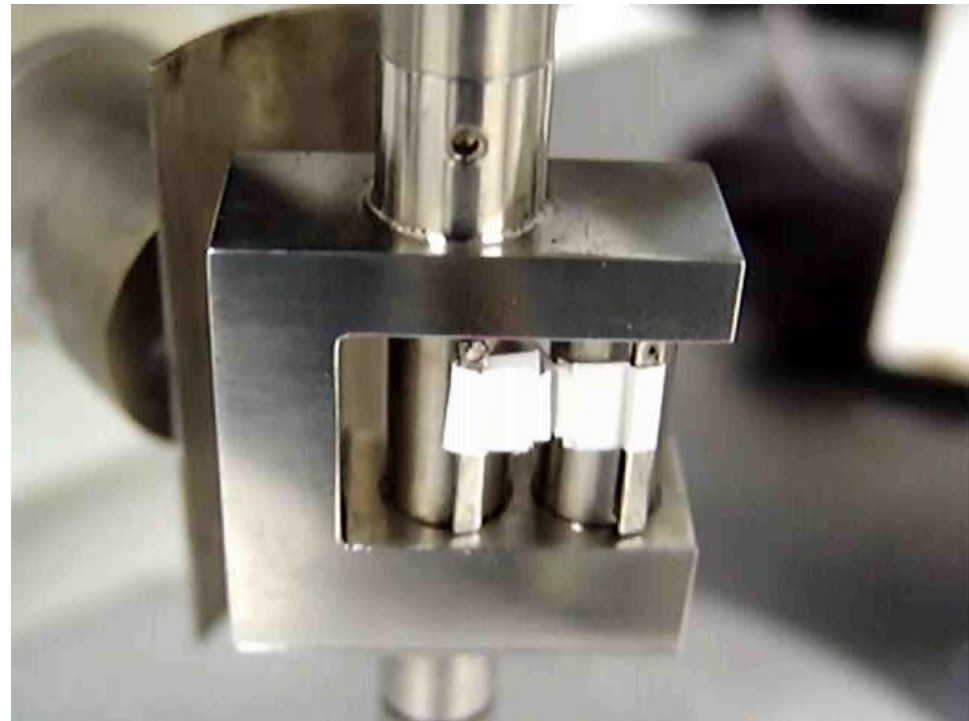
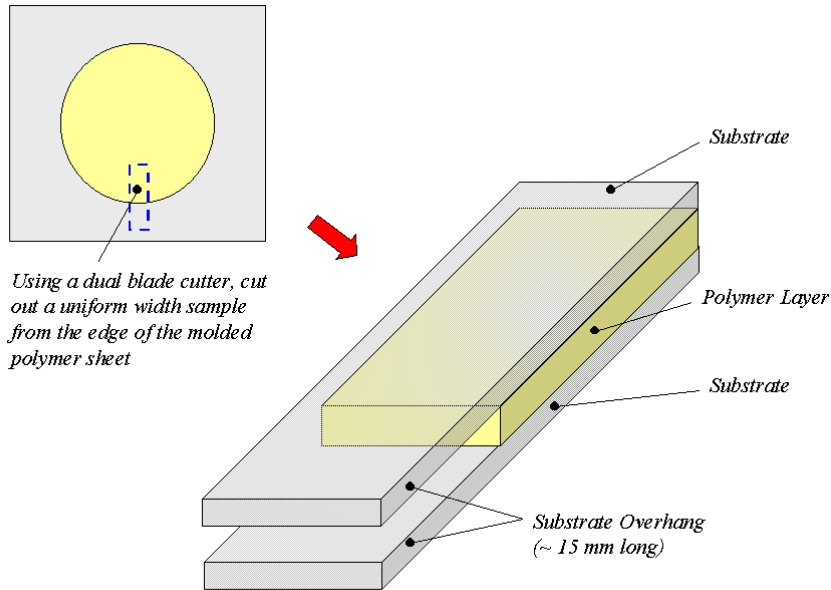
- Both LDPEs exhibit significant deviation from LVE behavior at large strains
- Despite having a much lower LVE melt viscosity the coating grade LDPE exhibits peak stresses almost equal to the film grade LDPE



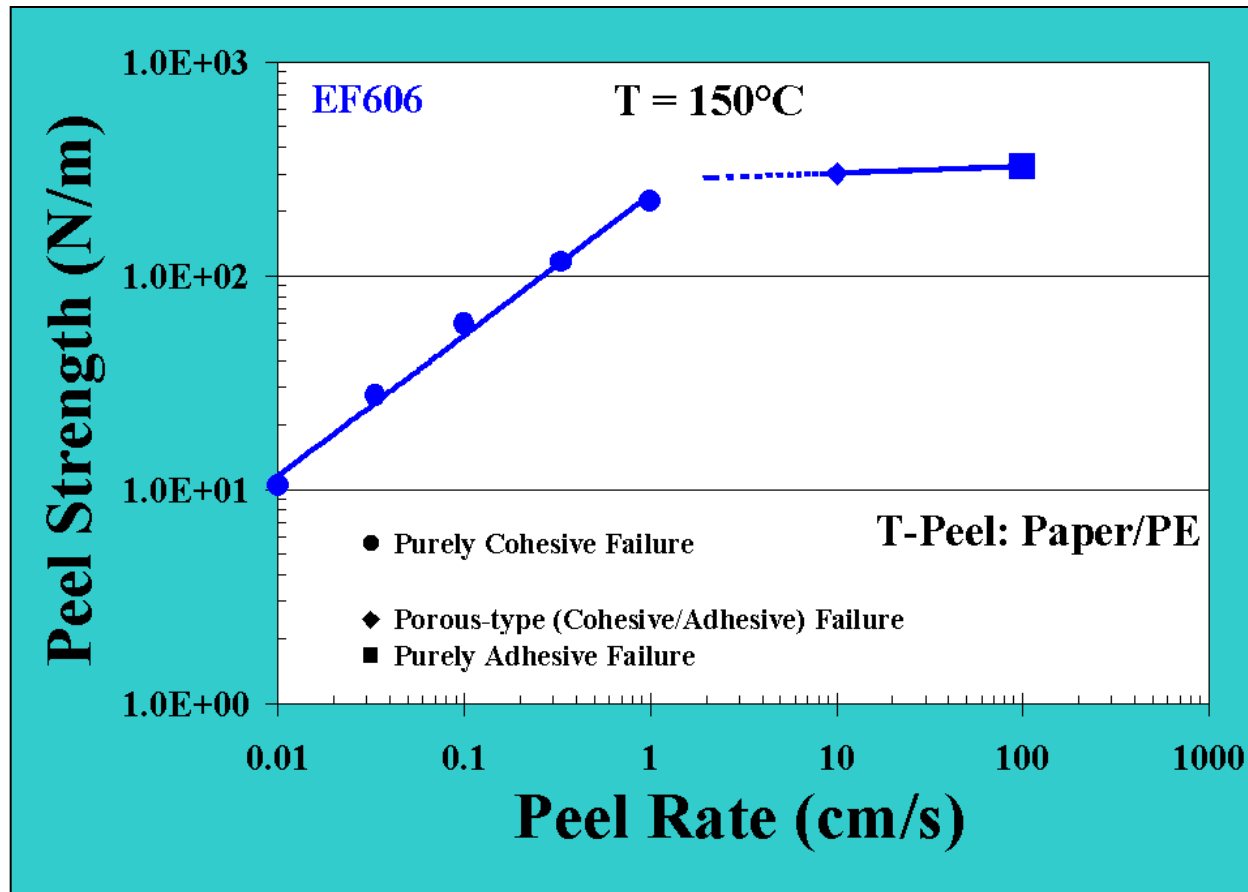
- Both LLDPEs exhibit little deviation from LVE behavior at low rates
- Both polymers exhibit increasingly elastic/rubbery behavior at very high rates and strains, with the Exact 3128 melt displaying significantly higher stress growth

Case Study 5: Dynamic Melt Adhesion Experiments

- PE peel specimens were prepared by molding polymer samples between sheets of plane white paper
- Specimens were cut-to-width (0.25") using a dual blade cutter
- The peel specimens were loaded onto the SER by securing the ends of the strips of paper to the windup drums, resulting in a T-peel configuration
- Peel rates: 0.01 to 200 cm/s @ 150°C



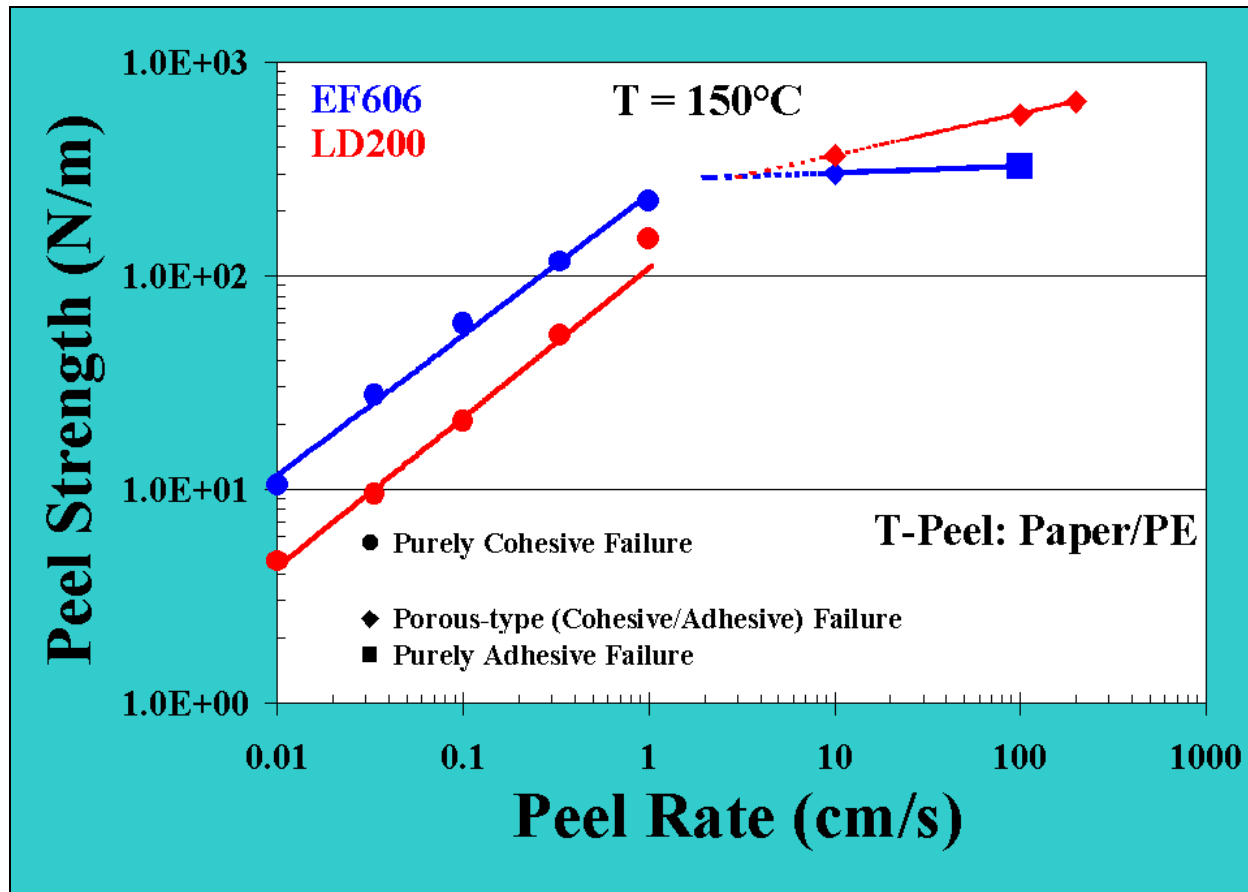
Case Study 5: Peel/Melt Adhesion Data



- The peel strength curve of the film grade LDPE (EF606) has very distinct regions of peel behavior as indicated
- Despite adhesive failure, peel strength always increases with rate



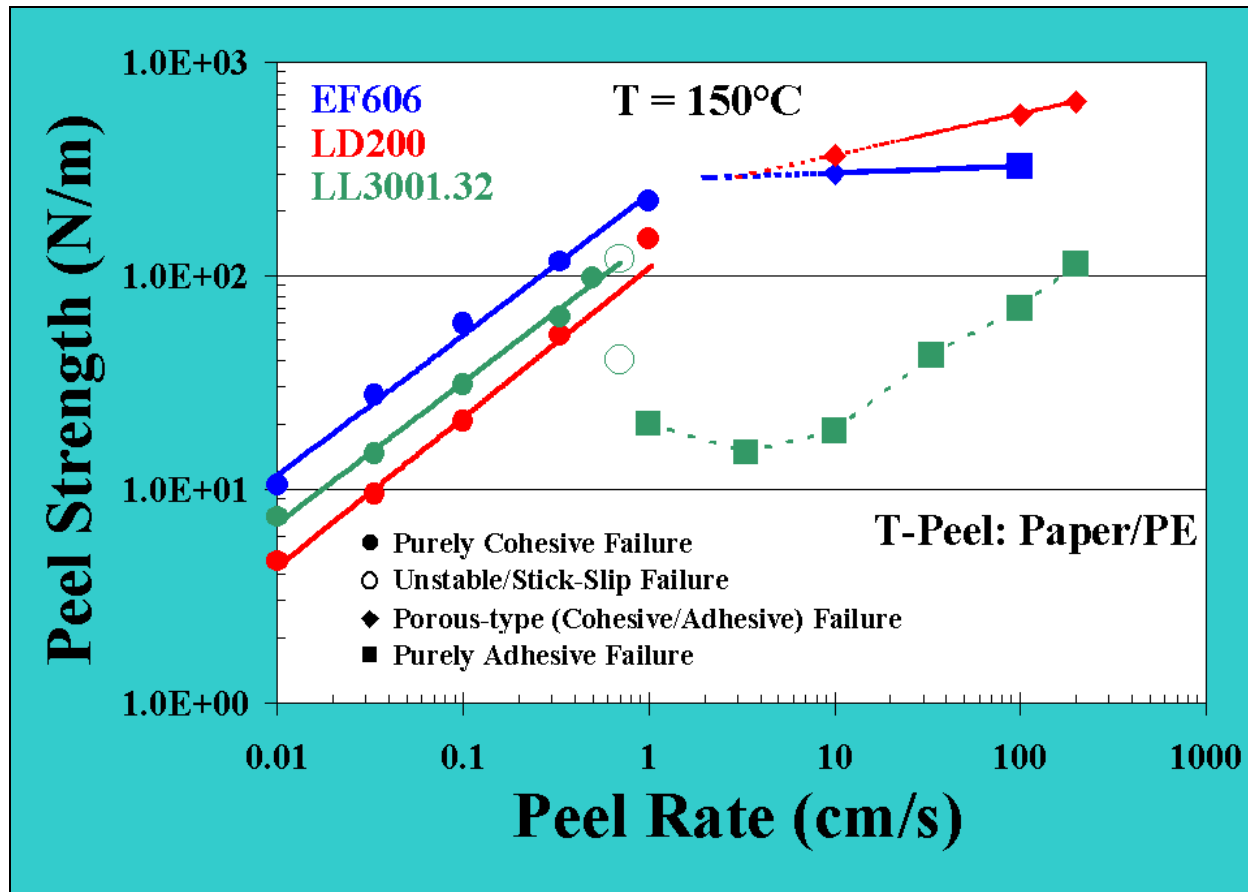
Case Study 5: Peel/Melt Adhesion Data



- The coating grade LDPE (LD200) also has a distinct “break” in the peel strength curve but exhibits superior peel strength to EF606
- LD200 does not exhibit adhesive failure



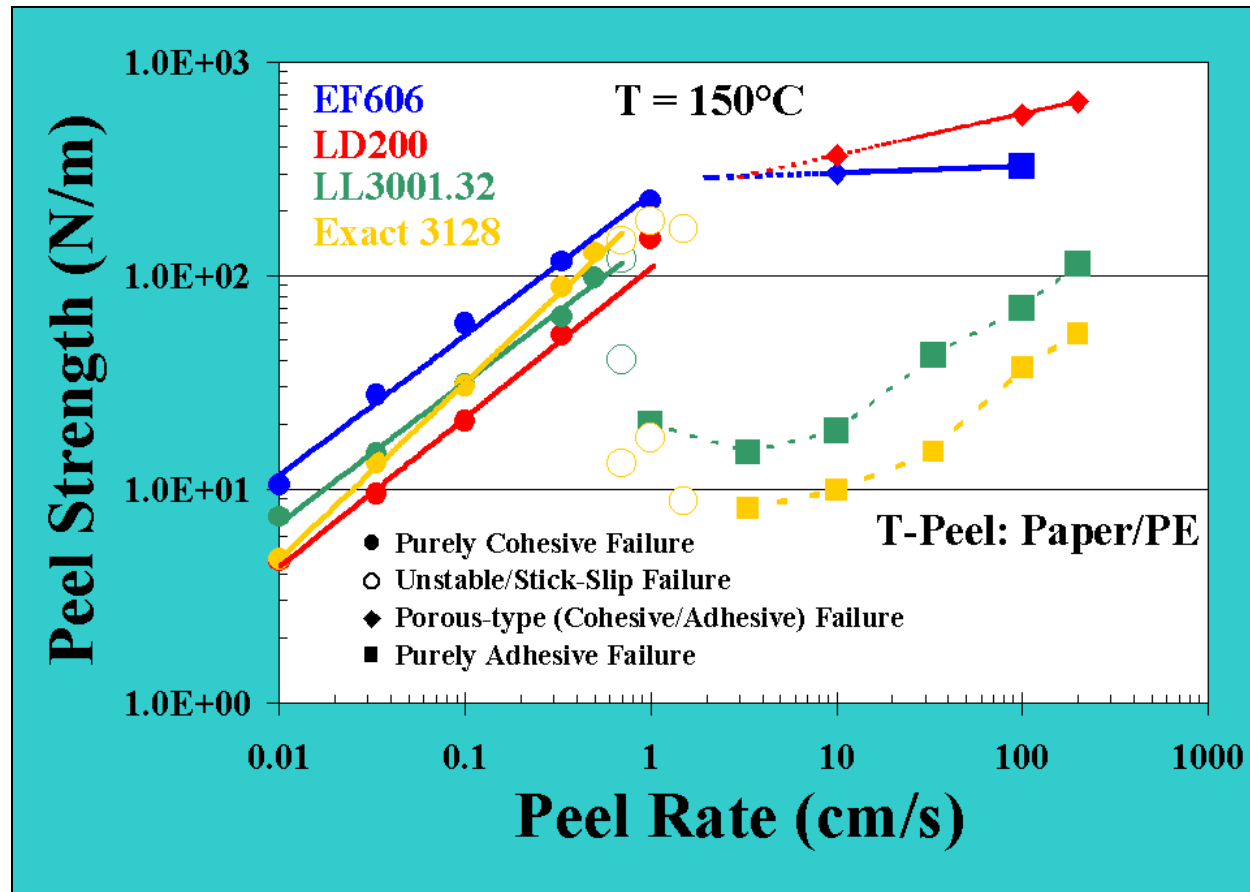
Case Study 5: Peel/Melt Adhesion Data



- The LLDPE (LL3001.32) exhibits an unstable region of peel behavior that appears qualitatively similar to stick/slip flow behavior
- Upon adhesive failure, peel strength drops dramatically



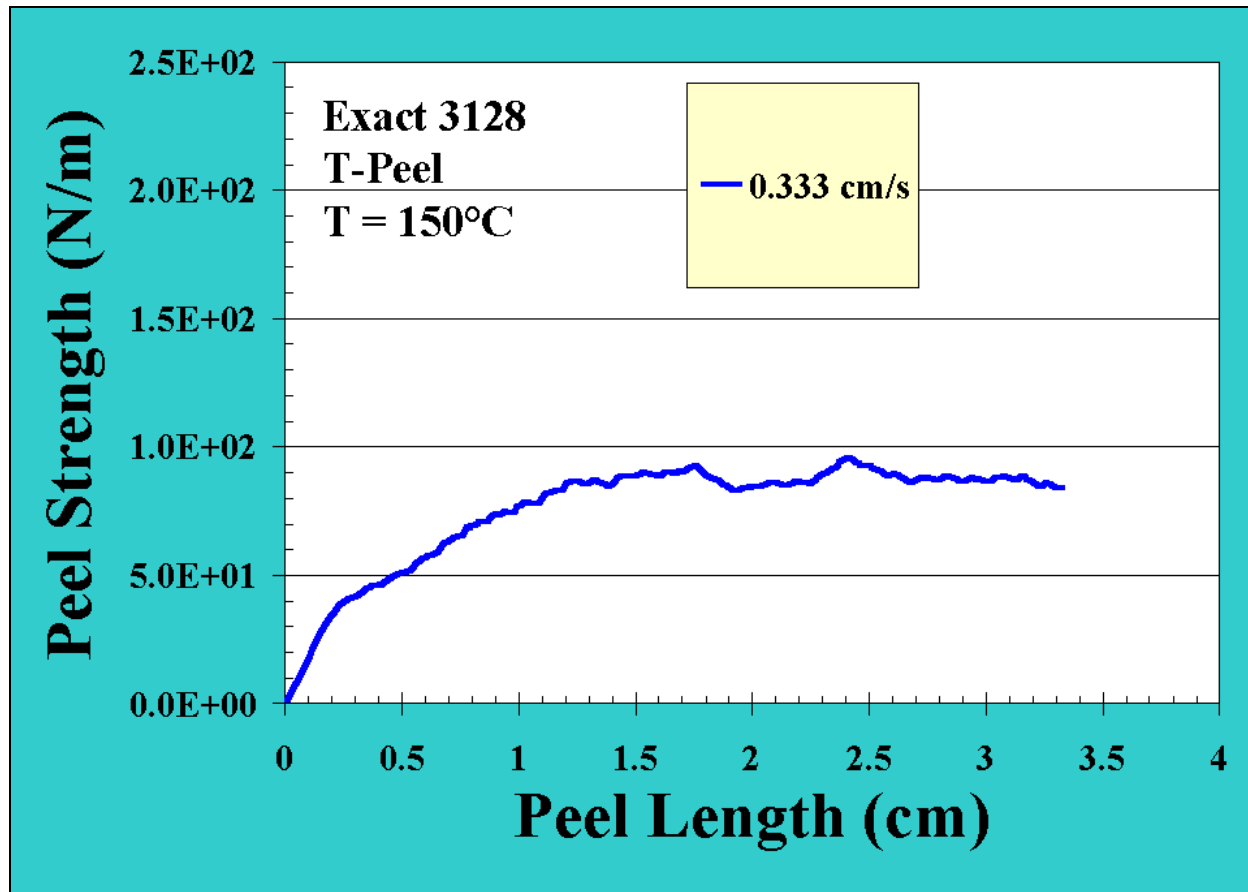
Case Study 5: Peel/Melt Adhesion Data



- Exact 3128 exhibits a larger region of peel instability that is very similar to its broad stick/slip flow region in extrusion
- Upon adhesive failure, peel strength decreases even more dramatically



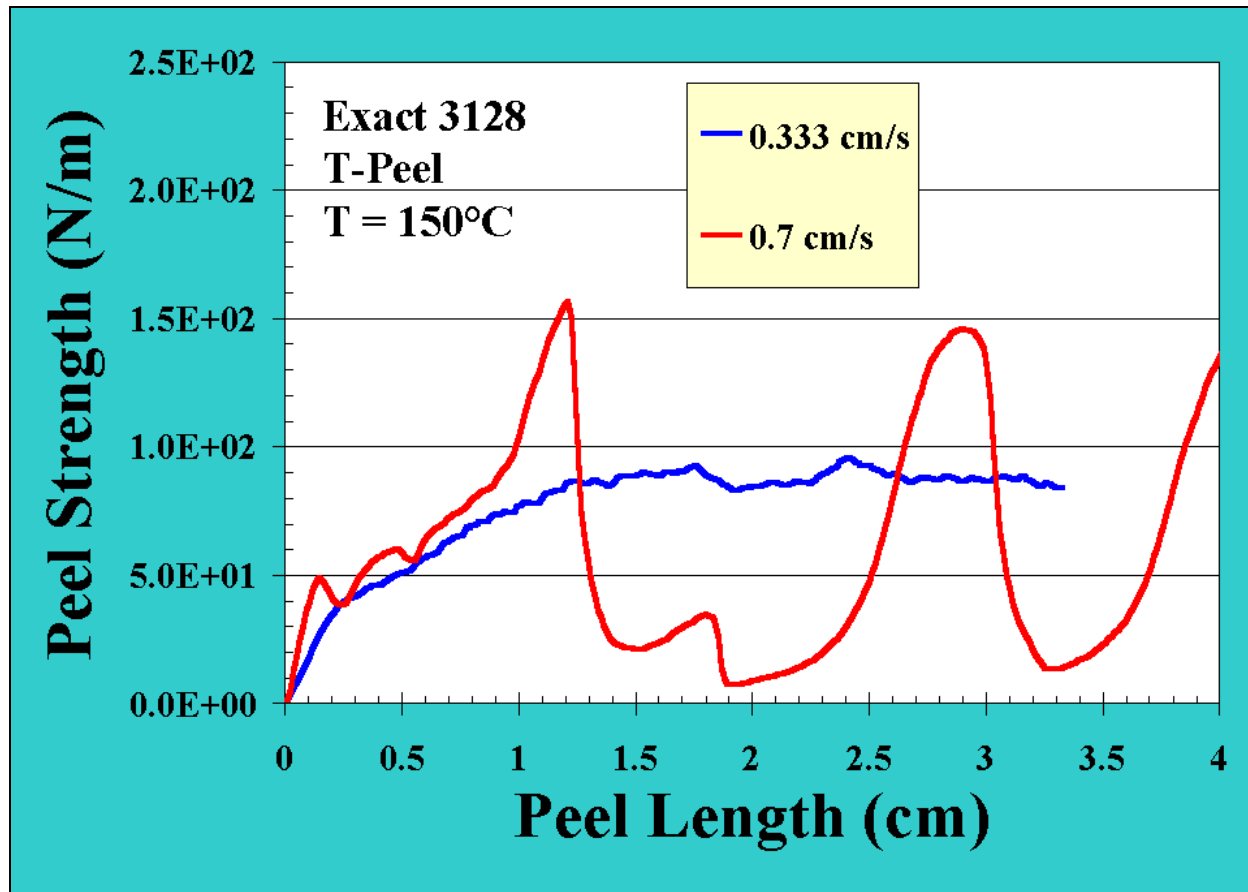
Case Study 5: Exact 3128 Peel Traces



- At a peel rate of 0.333 cm/s, the peel strength trace for Exact 3128 is stable and the peel failure is purely cohesive.



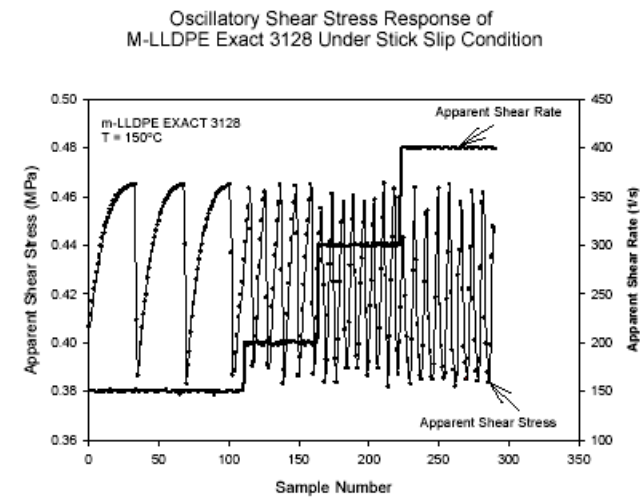
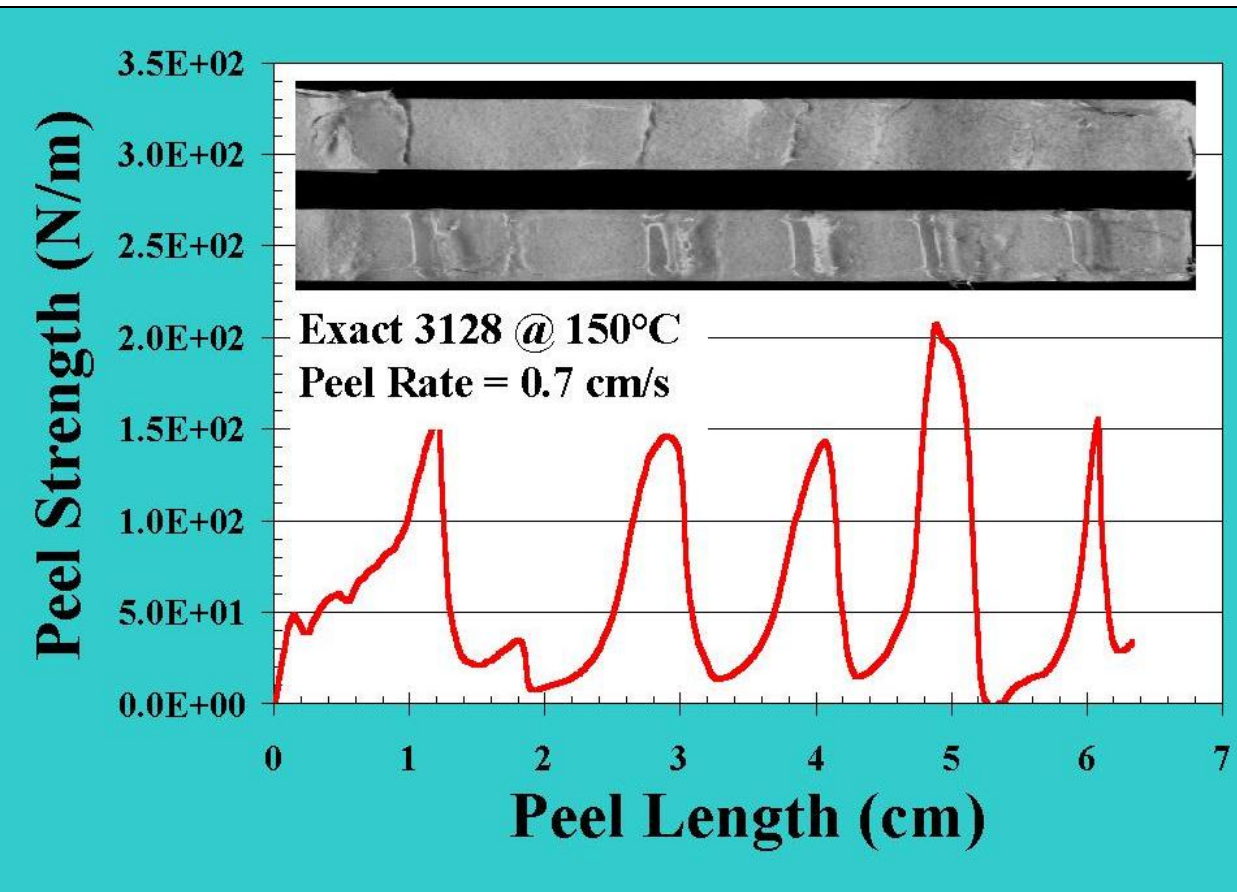
Case Study 5: Exact 3128 Peel Traces



- At a peel rate of 0.7 cm/s, the peel strength trace for Exact 3128 becomes unstable accompanied by an instability in the mode of failure.

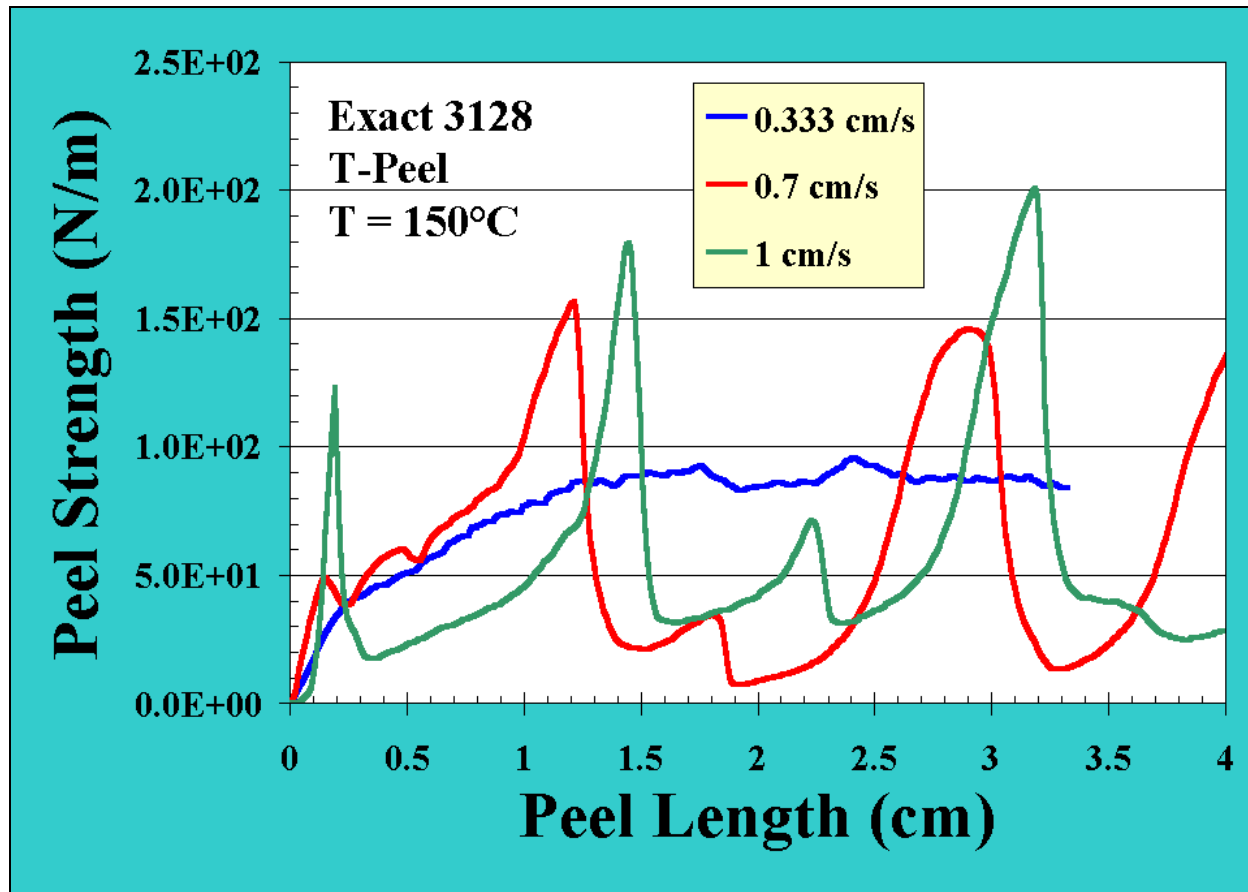


Case Study 5: Exact 3128 Peel Traces



- The peaks in the peel strength trace correspond to cohesive modes of failure and are abruptly followed by troughs corresponding to adhesive modes of failure.

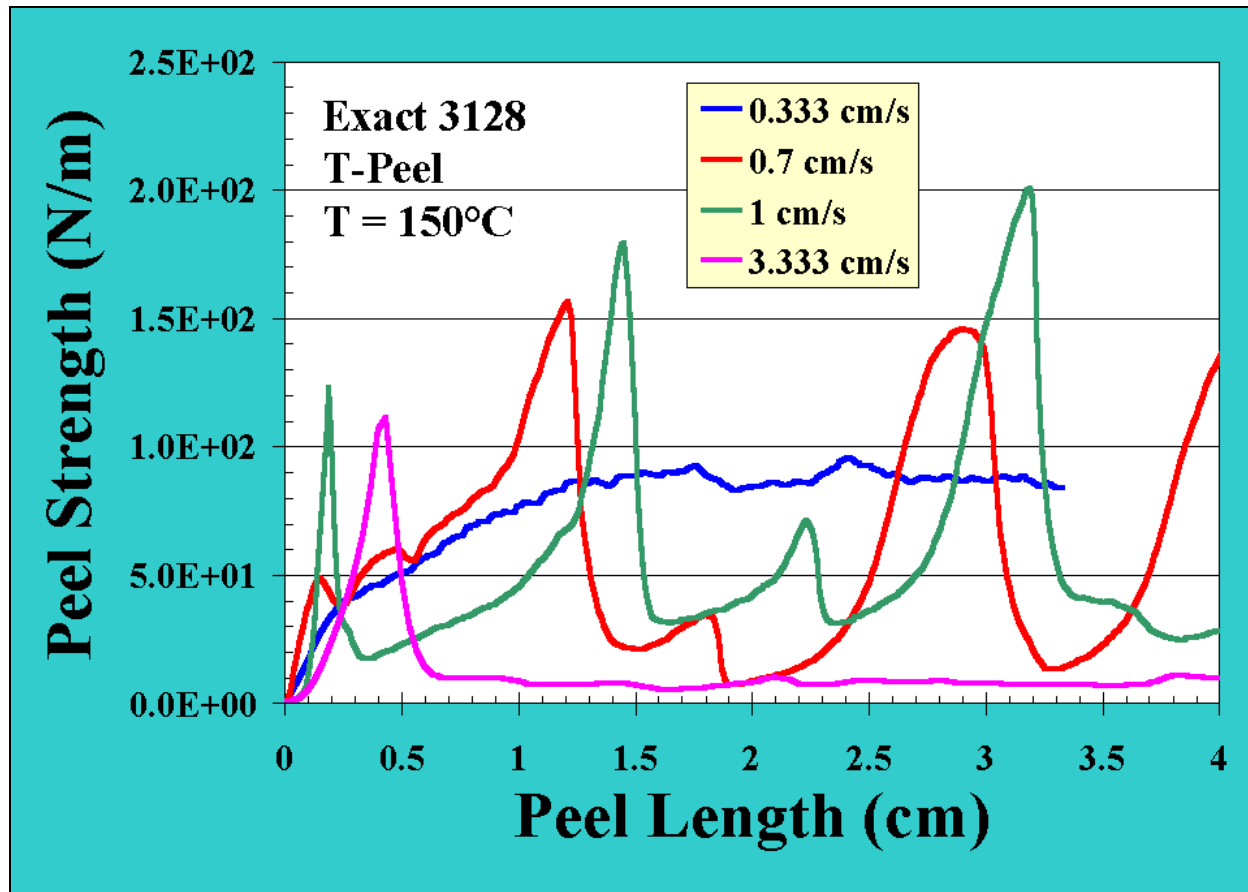
Case Study 5: Exact 3128 Peel Traces



- At a peel rate of 1 cm/s, the peel strength trace and mode of failure remains unstable.



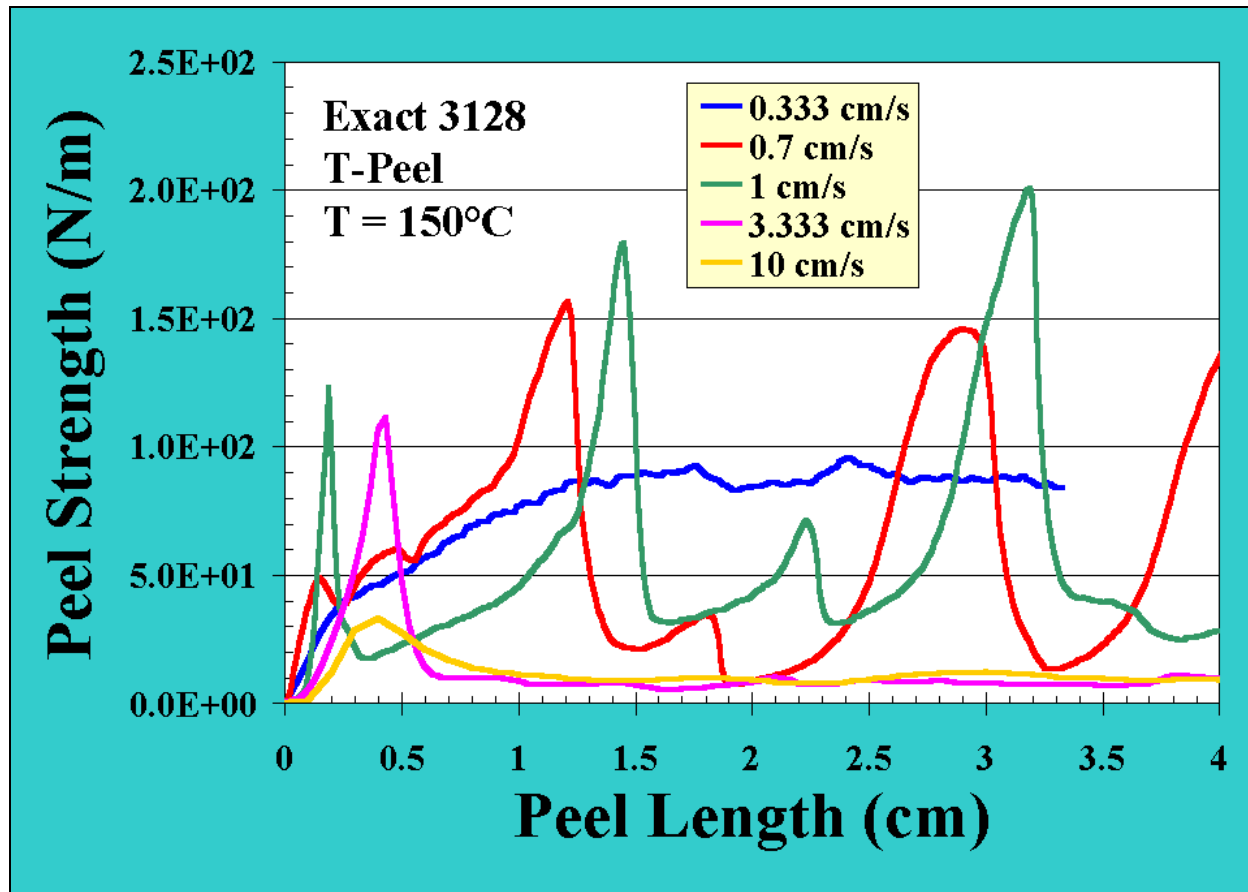
Case Study 5: Exact 3128 Peel Traces



- At a peel rate of 3.333 cm/s, the peel strength trace exhibits a brief peak followed by a significant drop in signal that remains steady - the mode of failure is purely adhesive.



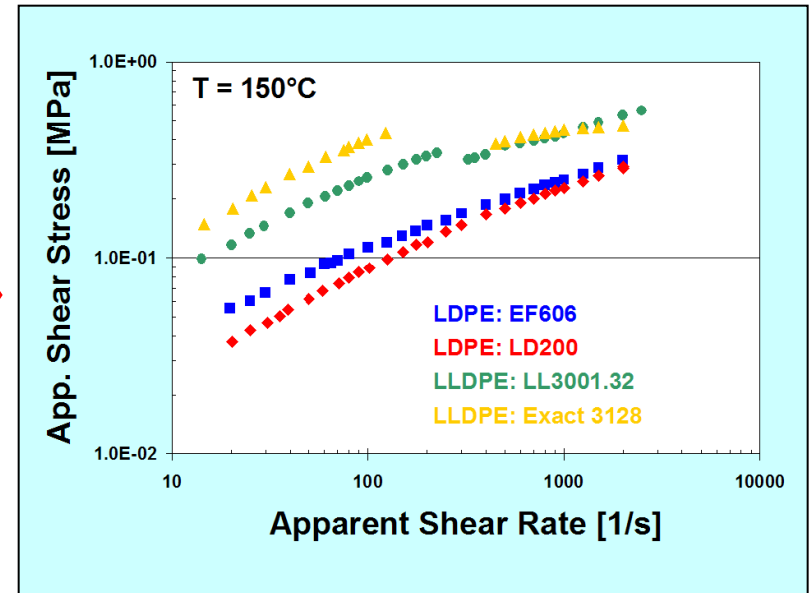
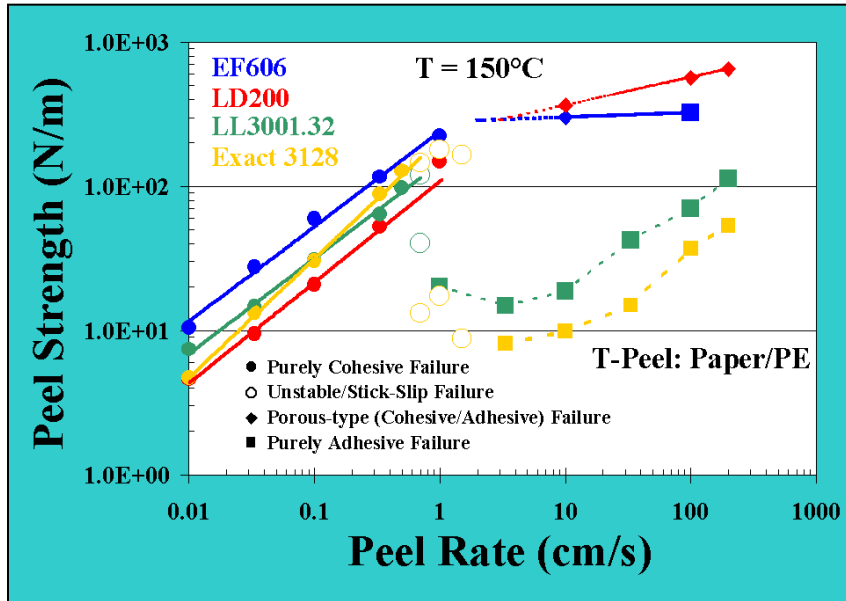
Case Study 5: Exact 3128 Peel Traces



- At a peel rate of 10 cm/s, the initial peel strength peak is greatly reduced and followed by a stable signal identical to the steady signal at 3.333 cm/s - the mode of failure is again purely adhesive.



Case Study 5: Insight into Processing Behavior



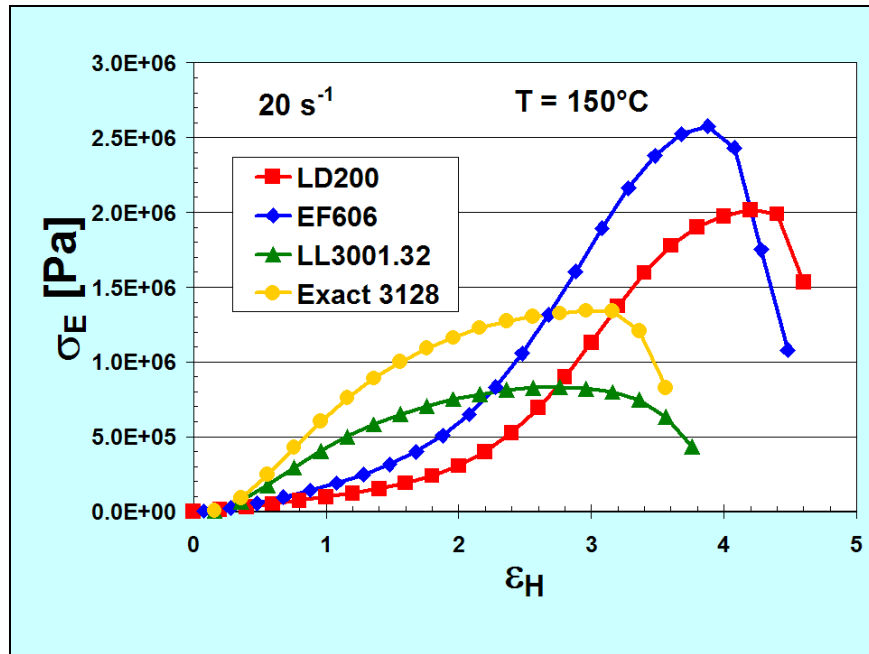
■ These melt peel results with the SER appear quite promising as a fingerprint/laboratory predictor of melt processing behavior and may provide fundamental insight into the role of adhesion/slip in melt flow instabilities.

Case Study 5: Dynamic Work of Adhesion...

- By characterizing the dynamic peel behavior of polymer melts against a variety of thin film substrates (metal foils, teflon films, etc.), one may gain insight into dynamic work of adhesion at rates relevant to processing.



Case Study 5: High-Rate Tensile and Melt Fracture Behavior



Critical Shear Rates for onset of...

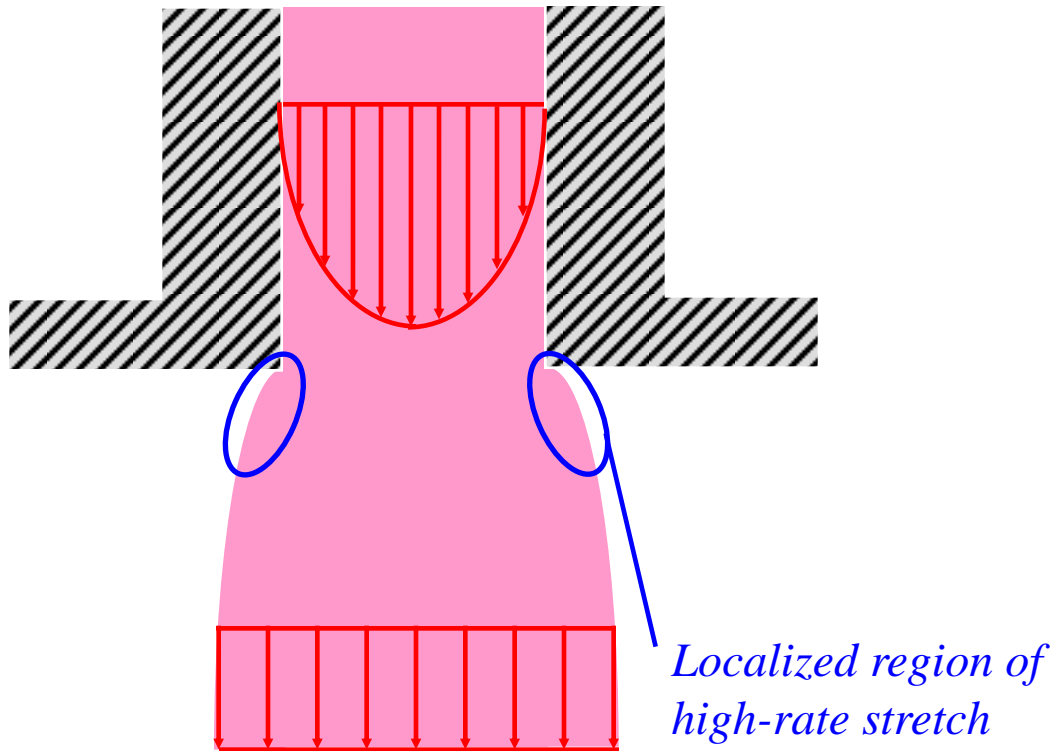
| <i>Polymer</i> | <i>Sharkskin</i> | <i>Stick-slip</i> | <i>Gross MF</i> |
|----------------|------------------|-------------------|-----------------|
| Exact 3128 | 20 | 120 | 420 |
| LL3001.32 | 70 | 240 | 1400 |
| LD200 | - | - | 270 |
| EF606 | - | - | 50 |

- High-rate tensile melt flow results appear to provide fundamental insight into the role of extensional flow behavior in processability and melt fracture phenomena.



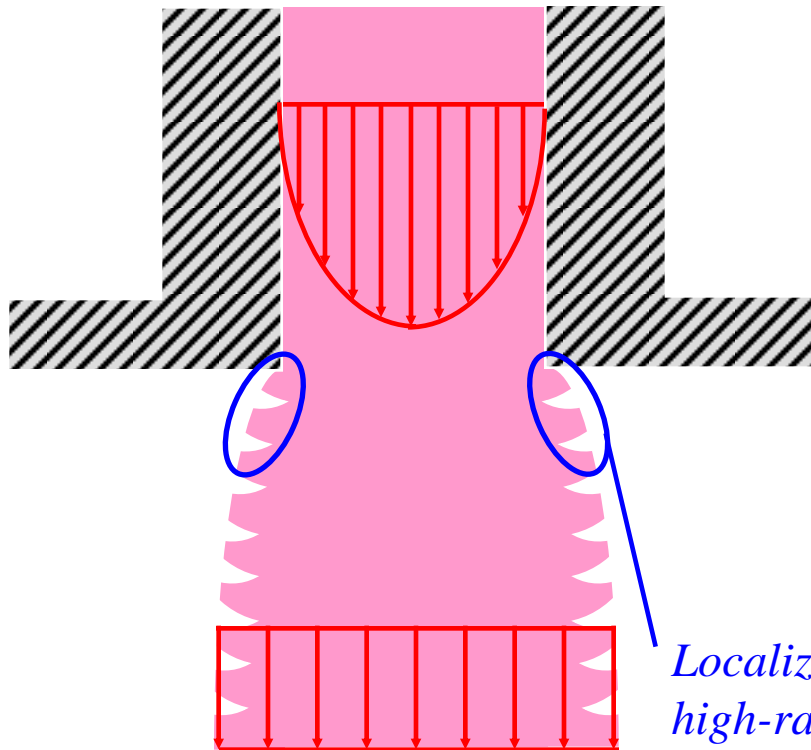
Case Study 5: Sharkskin Melt Fracture

- Exit phenomenon - stress governed flow



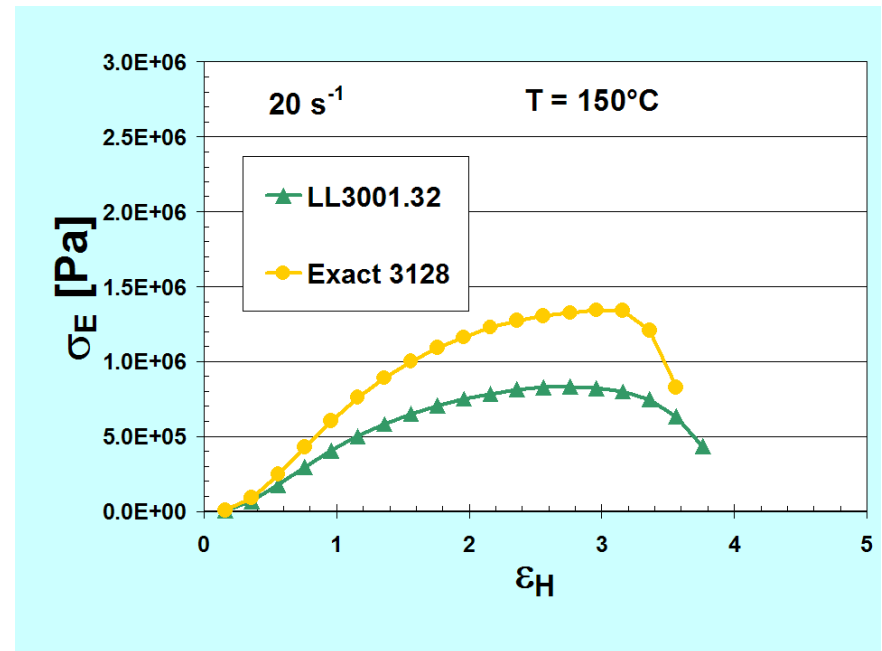
Case Study 5: Sharkskin Melt Fracture

- Exit phenomenon - stress governed flow



Localized region of high-rate stretch

Exact 3128 exhibits a much more rapid stress rise at high extensional deformations that can only be dissipated in the form of melt rupture propagated at the extrudate surface

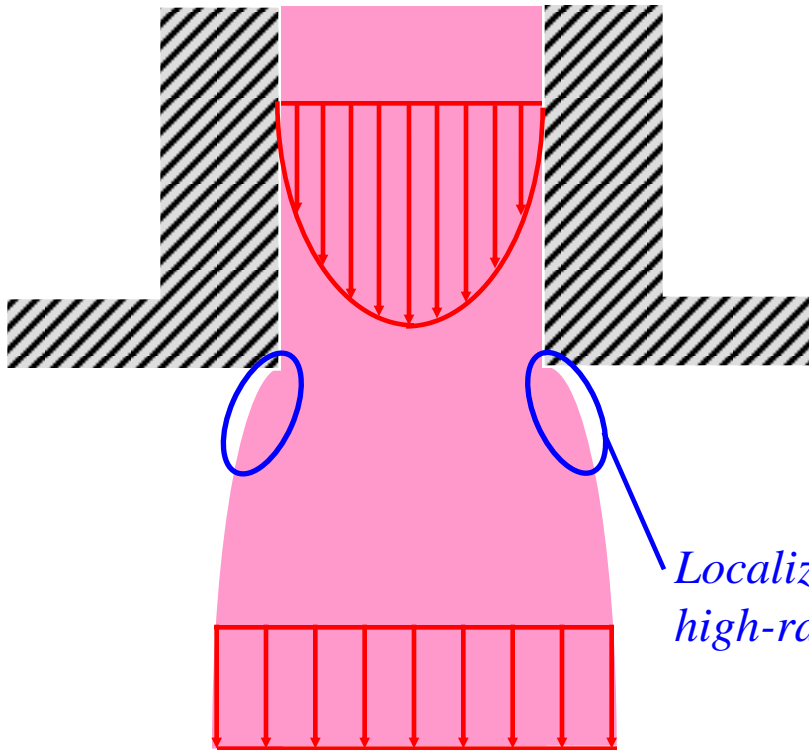


Critical Shear Rates for onset of...

| Polymer | Sharkskin |
|------------|-----------|
| Exact 3128 | 20 |
| LL3001.32 | 70 |

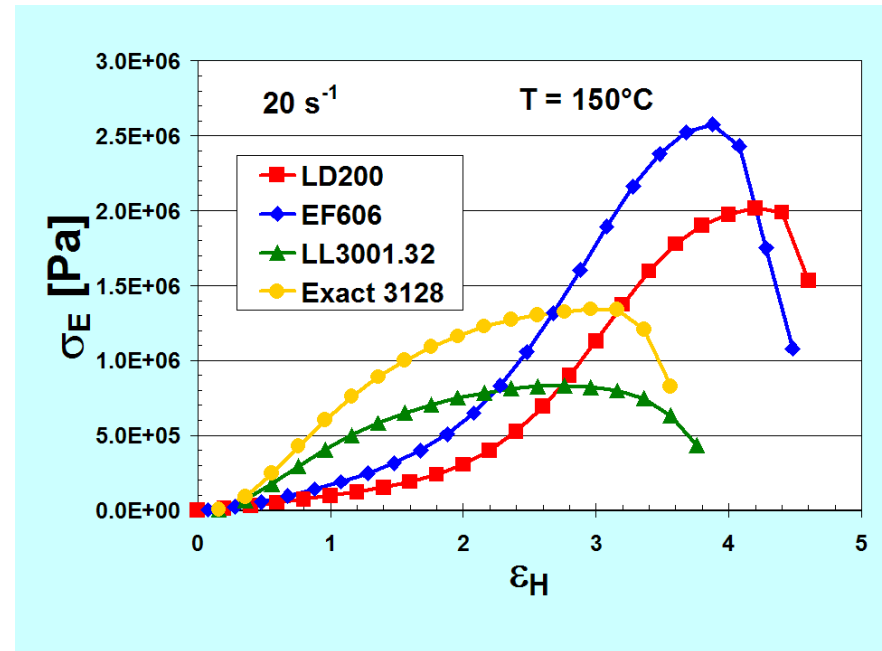
Case Study 5: Sharkskin Melt Fracture

- Exit phenomenon - stress governed flow



Localized region of high-rate stretch

The branched PE has an inherent stress retardation mechanism that enables stress to be rapidly dissipated upon exiting the die



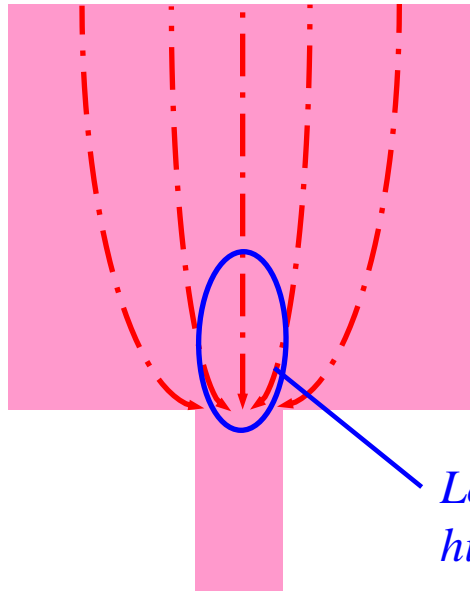
Critical Shear Rates for onset of...

| Polymer | Sharkskin |
|------------|-----------|
| Exact 3128 | 20 |
| LL3001.32 | 70 |
| LD200 | - |
| EF606 | - |

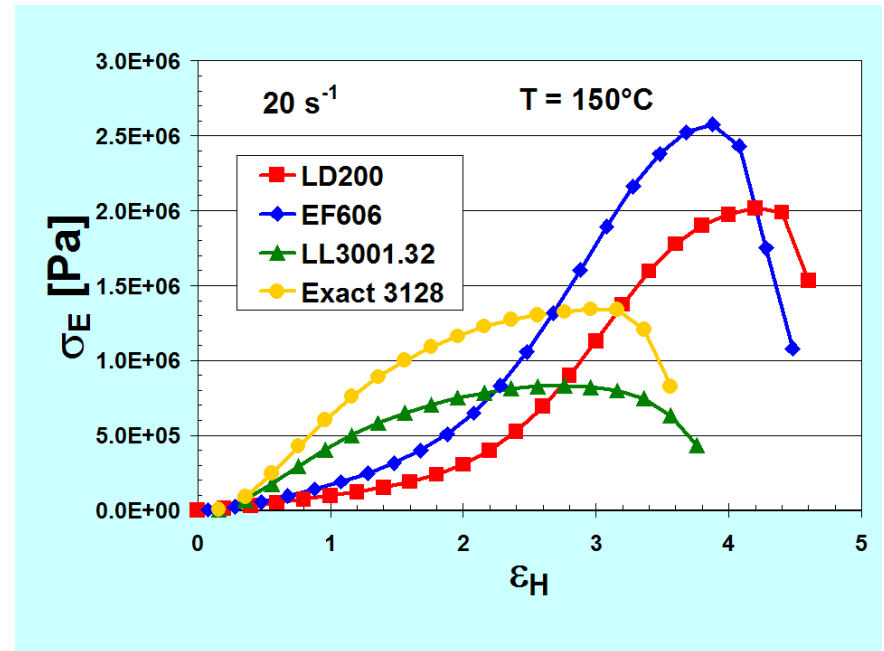
Case Study 5: Gross Melt Fracture

- Entrance phenomenon
 - strain governed flow

GMF occurs beyond a critical stress condition achieved in the die entrance flow region



Because the branched PE achieves higher stresses at elevated extensional strains, GMF is exhibited at an earlier onset in extrusion



Critical Shear Rates for onset of...

| Polymer | Sharkskin | Stick-slip | Gross MF |
|------------|-----------|------------|----------|
| Exact 3128 | 20 | 120 | 420 |
| LL3001.32 | 70 | 240 | 1400 |
| LD200 | - | - | 270 |
| EF606 | - | - | 50 |

Summary

- Because of the “strong” flow fields (providing high stretch and high orientation) generated, uniaxial extensional flows are very sensitive to flow induced crystallization effects in linear polymers and polymer macrostructure features in branched polymers
- Extensional rheology is a powerful method of material characterization providing a fundamental understanding of polymer structure/property relationships and valuable insight into polymer processing behavior

